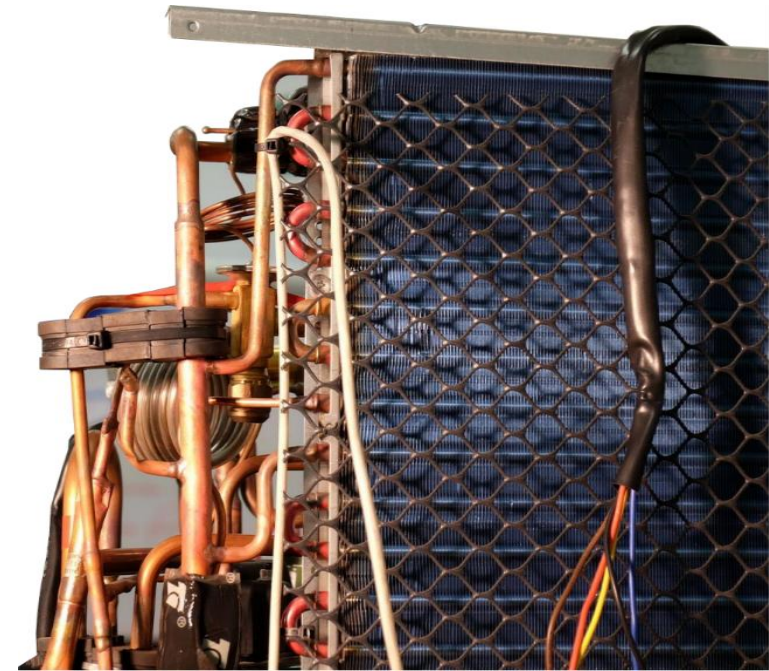


LIMITS OF MODELING APPROACH FOR REFRIGERANT CHARGE ASSESSMENT

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The necessity for smart HPs

- To support the deployment of HPs on the market, we need Smart HPs:
 - Real-time **performance** assessment
 - **Predictive maintenance** (soft faults)
- Why focus on **refrigerant leakage** ?
 - Soft fault with the **most important impact on HP performances**, but only after a certain loss of refrigerant (30-50 % of the nominal charge depending on the quality of the controls)
 - Also a **safety aspect** regarding flammable refrigerants → stringent safety regulations

Early detection of leakages and real-time quantification of the refrigerant charge is thus a major challenge.

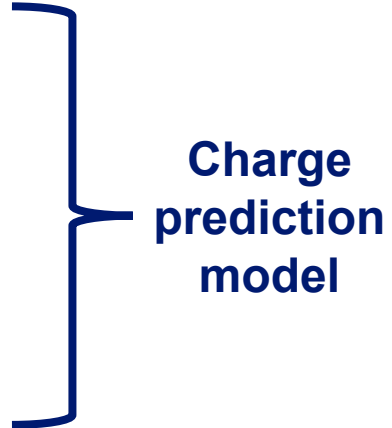
1. Context and objectives - Refrigerant charge prediction methods

- To **detect leakages**: monitor internal operating parameters of the HP (pressures, temperatures)

- To quantify:

$$\text{Refrigerant charge} = f(\text{Charge-sensitive feature, operating conditions})$$

Subcooling, evaporator inlet vapor quality Low and high pressures, compressor frequency...





Empirical approaches require **extensive experimental data**, across **multiple charge levels** AND **operating conditions**...



Why not use a **physical model of the HP** to generate **synthetic training data** for the charge prediction model ?

1. Context and objectives - Pros and cons of the different approaches

		
Empirical approach	<ul style="list-style-type: none"> • High accuracy 	<ul style="list-style-type: none"> • Large amount of experimental data across various conditions and charge levels • Difficulty to obtain high-quality experimental data → Time- and resource-consuming
Numerical approach, using a physical model of the HP	<ul style="list-style-type: none"> • Deeper understanding of HP behavior • Ability to cover any operating condition → a large amount of data can easily be generated • Can be validated using limited experimental data 	<ul style="list-style-type: none"> • Complex to develop • Deep knowledge of the system is required + information : <p>Dimensions & geometries: storage volumes are key in a closed-loop system</p>

1. Context and objectives – Objectives of the study



Necessity to accurately account for **all refrigerant storage volumes** and associated **physical phenomena**



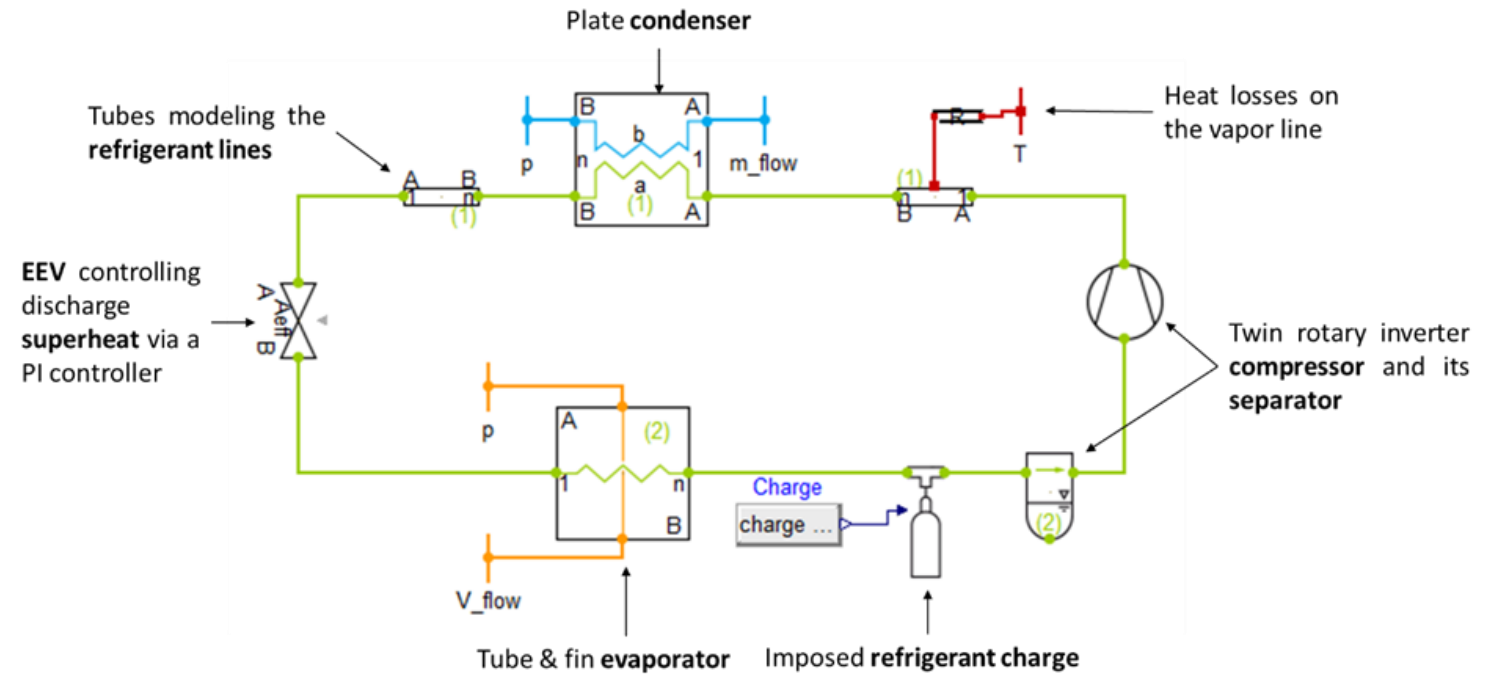
How can **uncertainties** or **simplifications** in the HP physical model affect the **reliability** of the resulting **charge estimation** ?



Assess the influence of the **physical model accuracy** on the overall **performance** of refrigerant **charge prediction** methods based on **model-generated data**

2. Methods – HP model and experimental validation

- **6 kW**
- **Split system**
- **R32**, nominal charge: **1,3 kg**
- Modeled using **Dymola + TIL library** → physical approach based on
 - **energy**,
 - **mass**,
 - **momentum balances**
 - exception: compressor → mapping of the efficiencies



Model validated against **experimental data**:

- Various **conditions**, **charge levels** 80-110 % of nominal charge
- **Steady-state** AND **dynamic** (HiL test bench)
- Errors < 5 %



Experimental observations:

- **No superheat** at compressor inlet (R32)
- **Very low subcooling**, 0 K for slightly undercharged system

2. Methods – Modeling key ancillary components for refrigerant storage

Condenser filter (~10-20 %)



Filled with filtering particles

? **Filling ratio**

→ Hypothesis: 60 %

Compressor crankcase and oil (~10 %)

? **Internal volume**

→ ~40% of compressor internal volume
(manufacturer data)



? **Refrigerant-oil solubility**

→ Tables available in literature

$Solubility = f(\text{discharge temperature} \ \& \ \text{pressure})$

→ Compromise for model efficiency:
fixed oil retention rate of 15 %

Suction accumulator (~40 %)

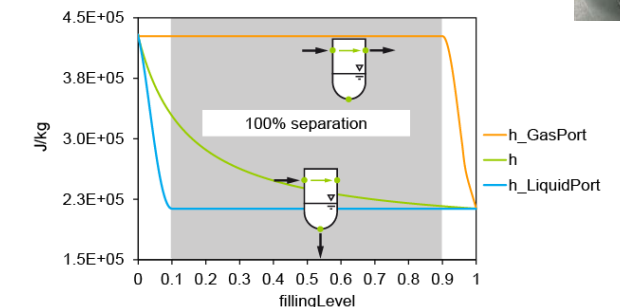
R32 → No superheat at compressor inlet
→ **key storage component**

? **Internal volume**

→ Manufacturer data

? **Liquid-vapor equilibrium**

→ Simplified approach:
ideal separation



→ Selected threshold:
80 % (arbitrary)



2. Methods – Charge prediction model, training and testing data



	Min	Max	Step
Refrigerant charge level (% of nominal charge)	80	110	2
Outdoor temperature (°C)	-10	10	5
Return water temperature (°C)	30	50	10
Compressor Frequency (Hz)	40	100	20

- Regression method: **Histogram Gradient Boosting (HGB)** regressor
→ Compromise between **accuracy** and **computational efficiency**
- **Charge-sensitive features: subcooling and evaporator inlet vapor quality**
- Operating features: **low and high pressures, compressor frequency**

2. Methods – In a nutshell

1

Reference model

→ perfect representation of the real system (no error)

→ a unique **reference testing dataset**

– operating conditions **randomly sampled** following a uniform distribution

(Training and) testing

2

Degraded models 1 component

Misestimation of the **filter's** internal volume

+ 10 %
- 10 %

Misestimation of the **crankcase's** internal volume

+ 25 %
- 25 %

Ideal separation thresholds in the **suction accumulator**

90 %
70 %

Training only

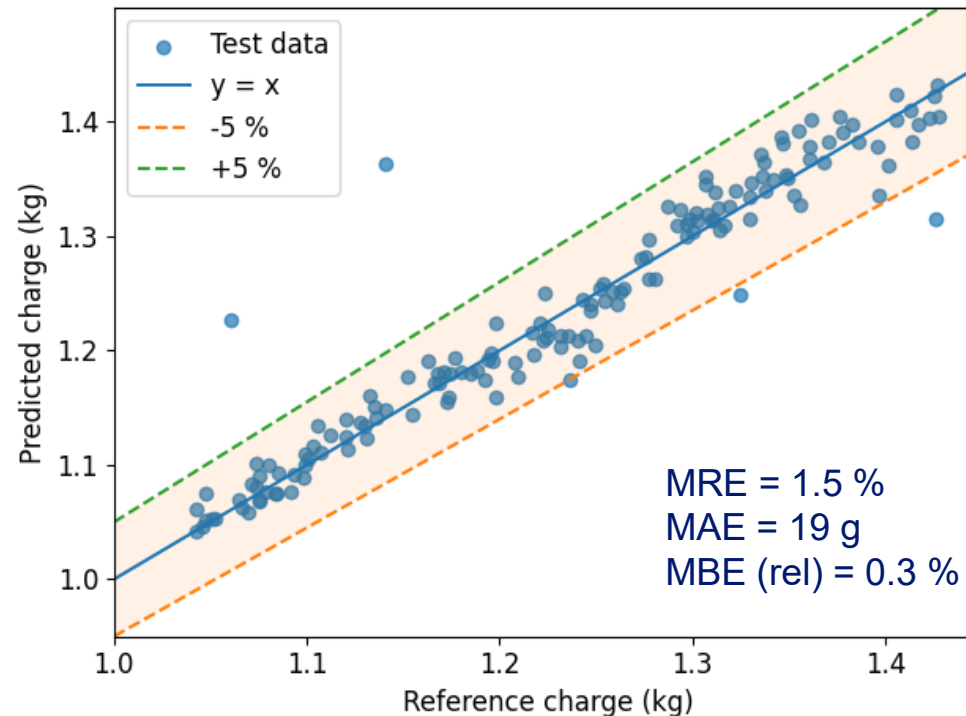
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Degraded models 2 components

- Filter **underestimation** / accumulator **overestimation**
- Filter **overestimation** / accumulator **overestimation**

3. Results and discussion - Reference scenario: training conducted on a perfect HP model

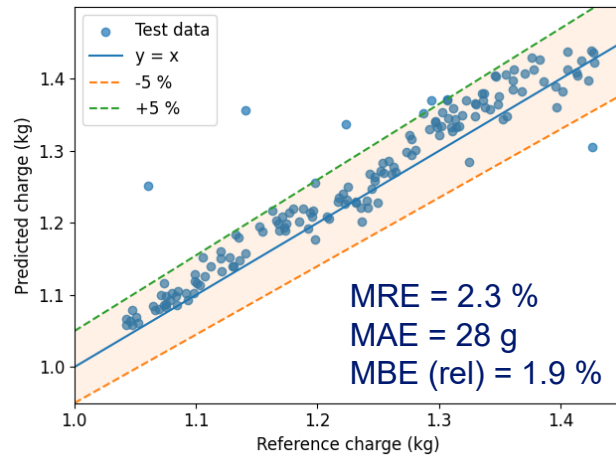
Charge prediction model **trained** using data generated by the **reference model** and tested on the **testing** dataset generated by the same model.



3. Results and discussion – Mischaracterization of one component

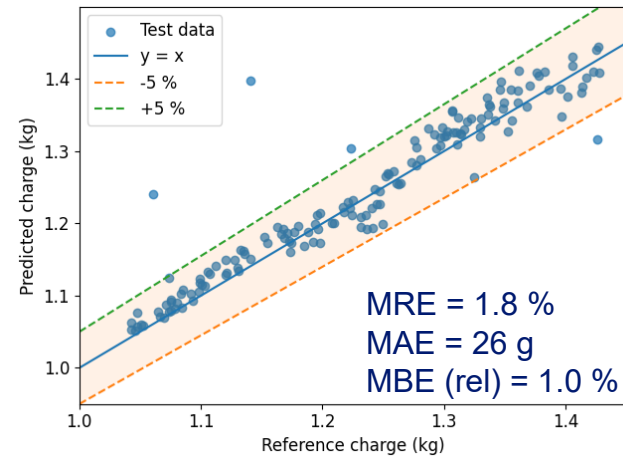
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Condenser filter



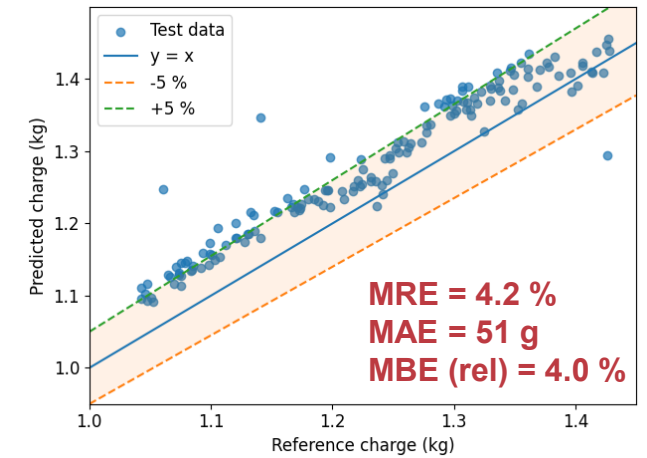
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Compressor crankcase and oil

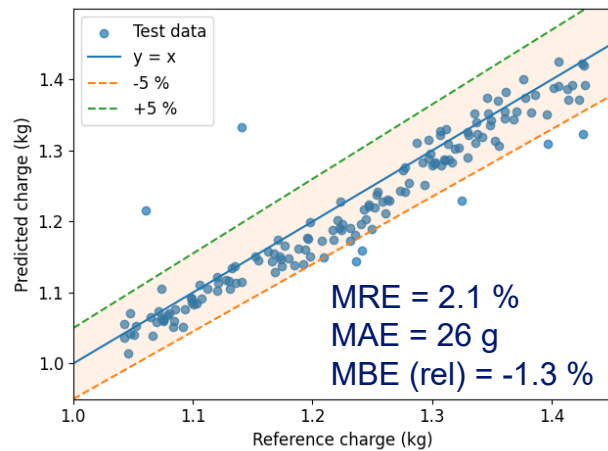


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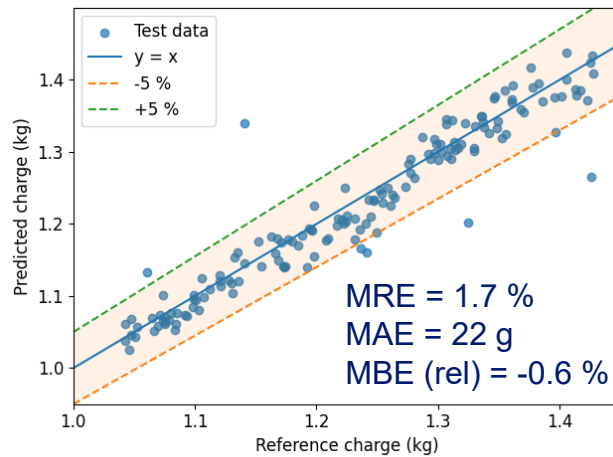
Suction accumulator



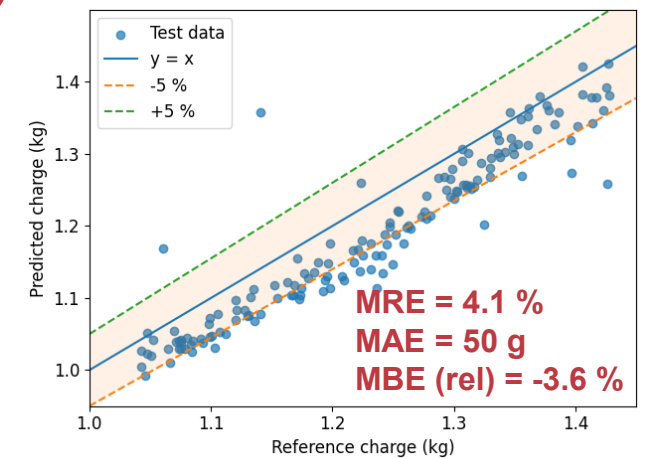
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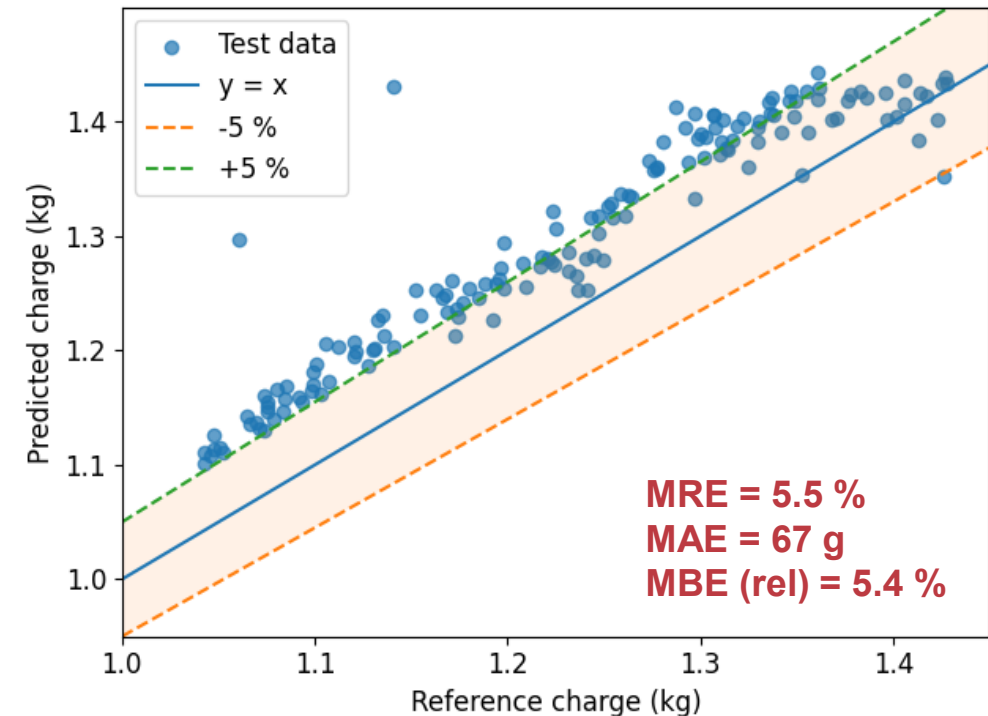
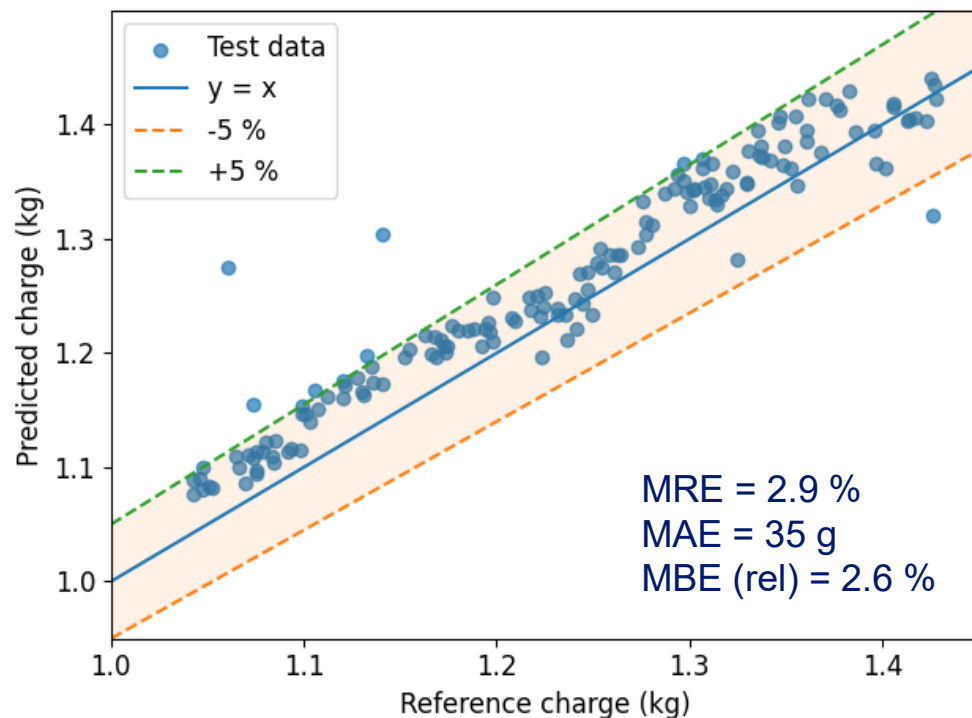
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3. Results and discussion – Mischaracterization of two components

– Condenser filter + Suction accumulator

+ Condenser filter + Suction accumulator

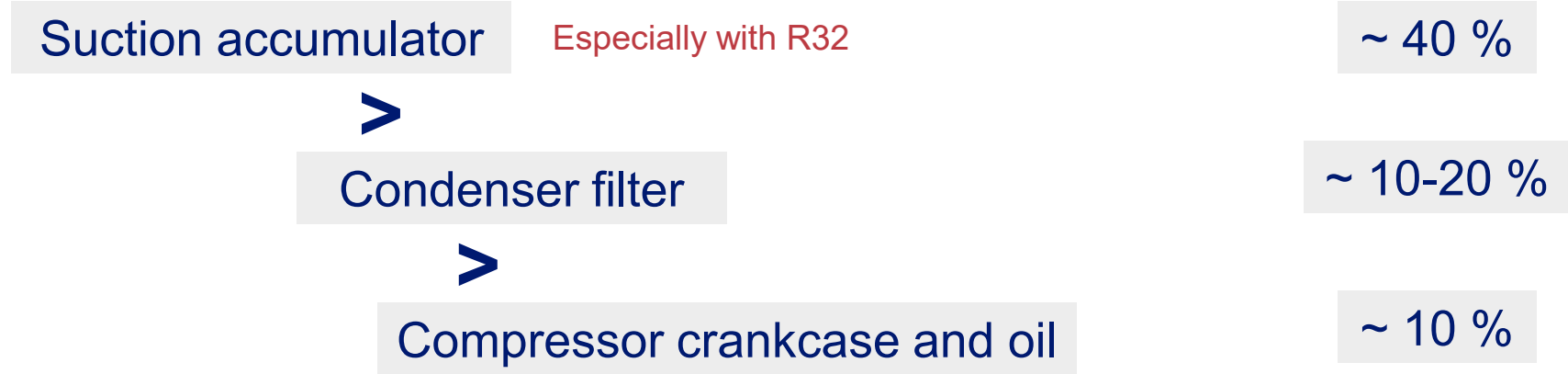


→ The errors can somehow **compensate** each other

→ But they can also **add up...**

3. Results and discussion – Summary

- Impact on charge prediction:



Consistent with refrigerant storage:

- Prediction performance** impacted by:
 - ~ 4 % for individual component error
 - **Up to 5.5 % with multiple errors**
- Even though the error may remain **acceptable**: the model will **systematically under- or overpredict** the refrigerant charge

4. Conclusion & Perspectives



Can **model-generated data** support **refrigerant charge prediction** ?

Physical model of an R32 HP treated as an **ideal representation** of the real system



Degraded models with **mischaracterized** components

↳ (Training data +) **testing data**

↳ **Training data**

- Modeling of **suction accumulator**: particularly **critical** (compared to filter or compressor crankcase)
- If multiple components mischaracterized: error **up to 5.5 %**
- Most cases: **acceptable error** → Difficult to draw definitive conclusions.



Accurately **modeling refrigerant distribution** for charge prediction in **closed-loop systems** is a **complex** task

→ Using **physical models** to generate **synthetic data** for **charge prediction** may be more **challenging** than anticipated.

4. Conclusion & Perspectives

Limits of the current approach and **perspectives**:

- Only a **subset of modeling uncertainties** are addressed
- **Dimensions** and **geometries** considered, but what about **correlations** ? Heat transfer, void fraction
 → Extend this work to other components, such as **heat exchangers**
- **Danger: if the errors add up !**
- Real systems may exhibit **more complex behaviors**, more so with **refrigerant storage phenomena** in **dynamic operation**



Model-generated data may support charge prediction **BUT:**

- This approach requires **deeper investigation** and **careful validation**.
- The **limitations of physical modeling** must be clearly understood before relying on it as a **substitute for experimental data**.