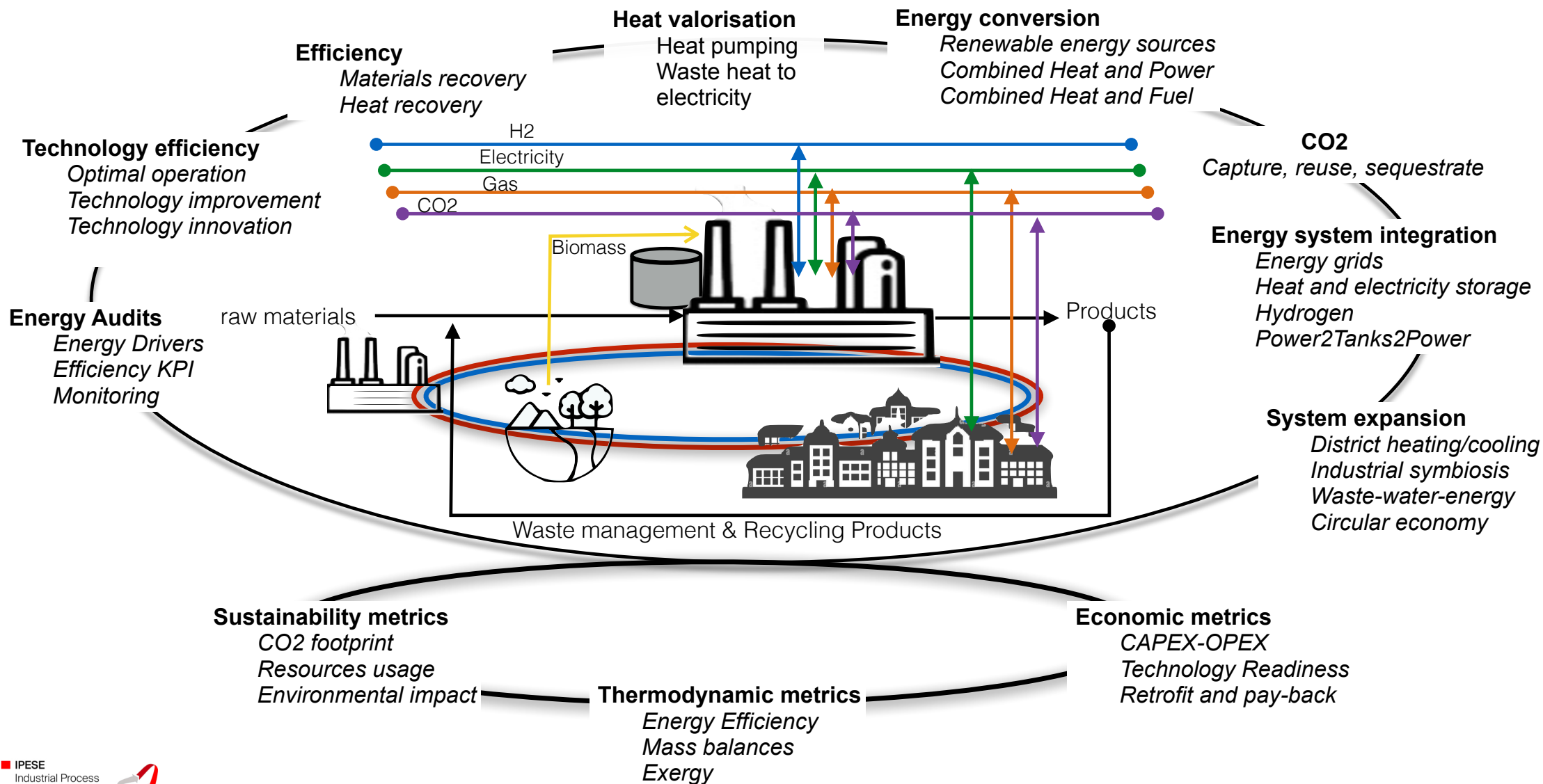


Efficiency Increase by Systematic Heat Pumping Integration in Industrial Processes

Prof François Maréchal
Industrial Process and
Energy Systems
Engineering
EPFL Valais-Wallis
Switzerland

EPFL Defossilizing industry : thematics

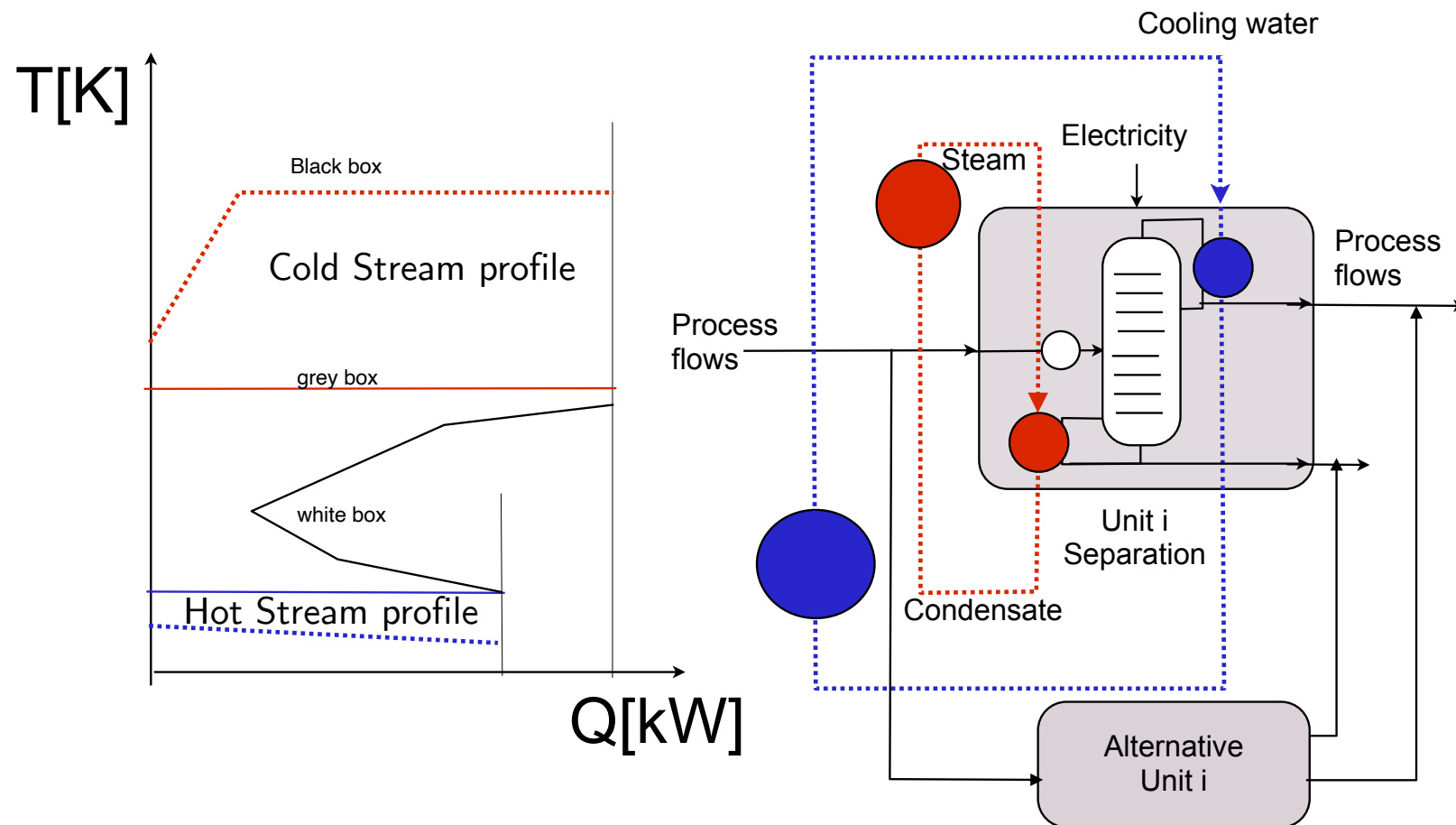
2



EPFL Unit Operation energetics : Heat transfer Interfaces

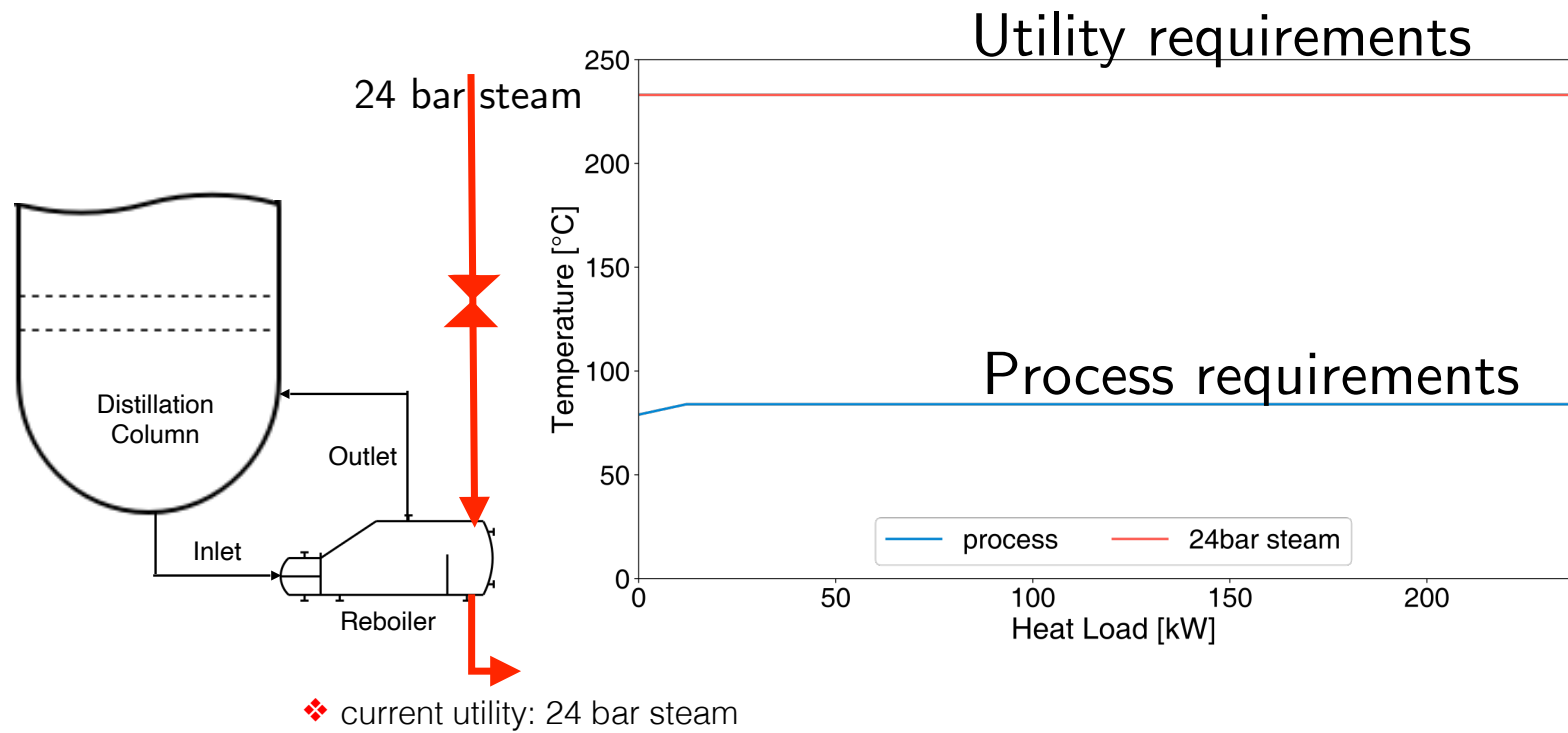
3

- Same unit operation : different heating and cooling profiles



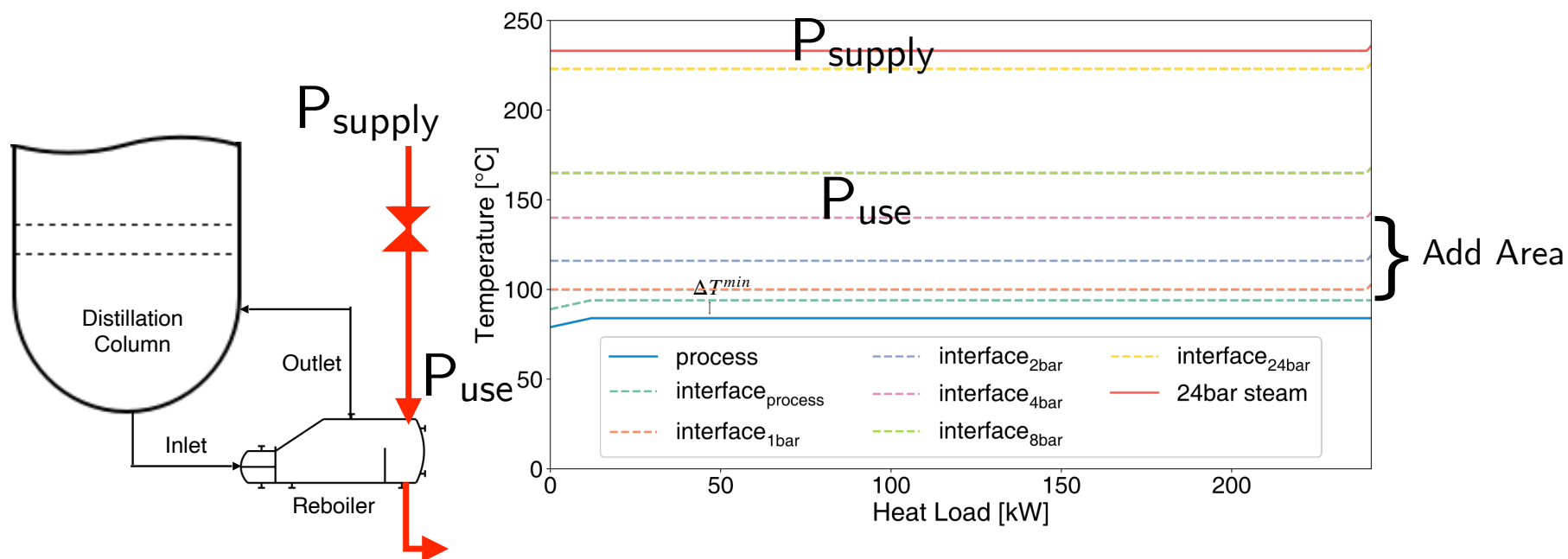
EPFL Heat exchanger transfer interfaces

4



EPFL Analysing heat transfer interfaces

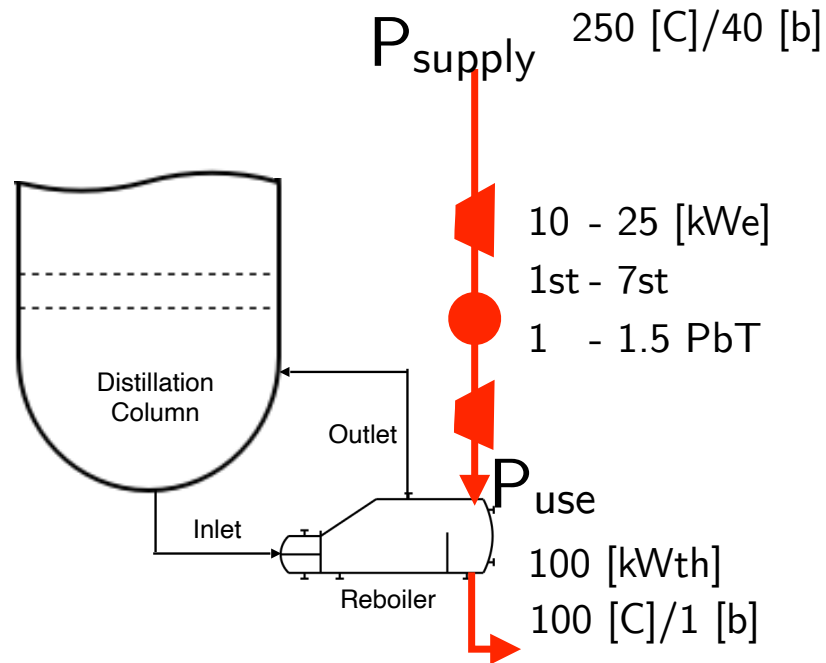
5



- ❖ current utility: 24 bar steam
- ❖ representation of the process with its current utility interface
 - ◆ allow the integration of only the current utility, or a higher temperature source
- ❖ Possible different heat exchange area => investment if $P_{supply} < P_{use}$

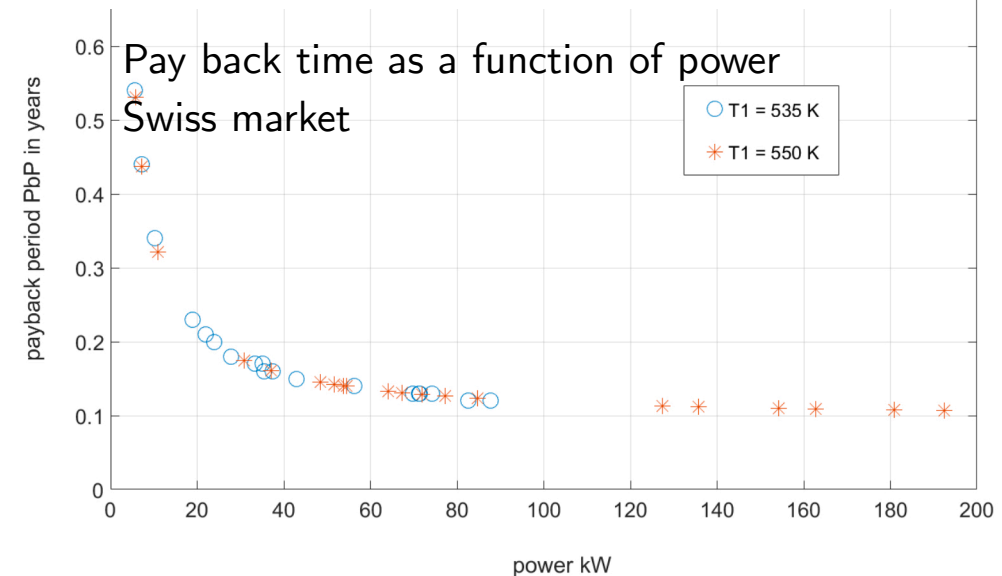
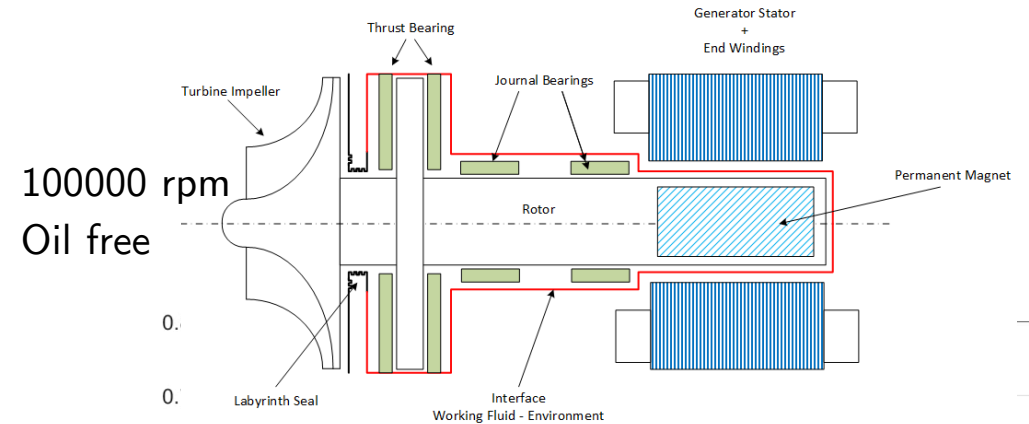
EPFL Replacing valves by Oil free Micro-Turbines

6



- ❖ Replace valves by micro turbines
- ❖ Pay back is low even for small flowrates
- ❖ multi stages => 3x the power but Pay Back *1.5

Micro-turbine design

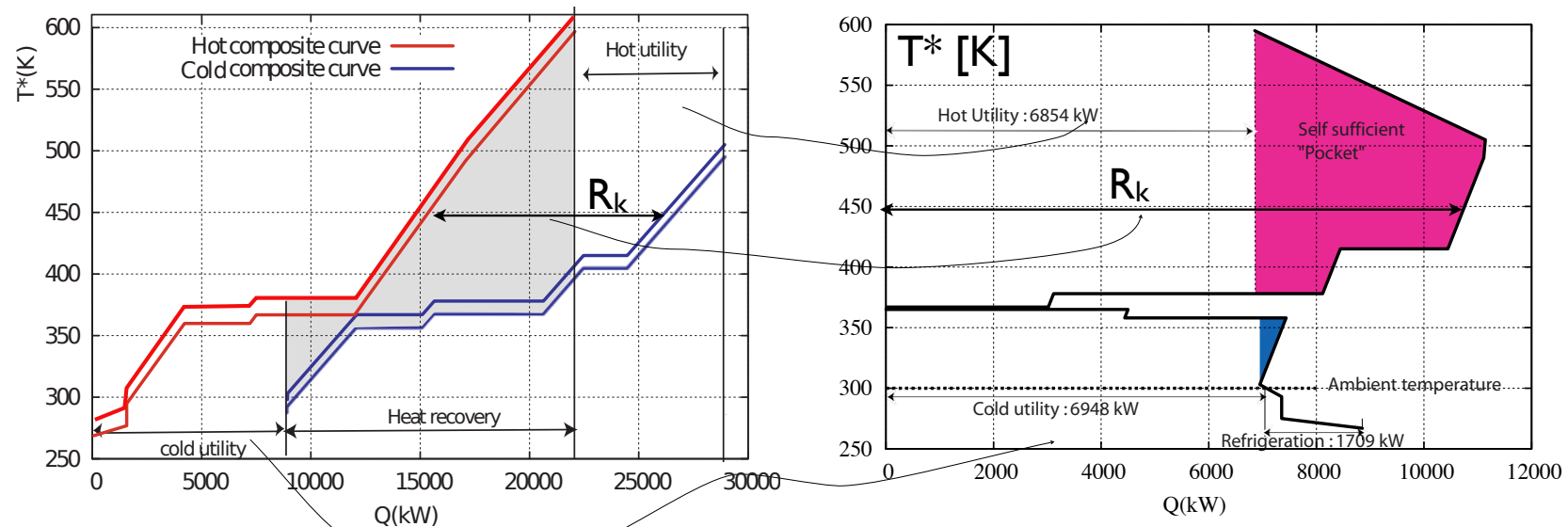


Weickgenannt A, Kantor I, Maréchal F, Schifffmann J. On the Application of Small-Scale Turbines in Industrial Steam Networks. Energies. 2021 Jan;14(11):3149.

EPFL Heat recovery and heat cascade

7

- Corrected temperature $T^* = T + / - (\Delta T_{min}/2)$
- Graphical plot of the heat cascade : $[R_r, T^*_r]$ $r=1, n_r$

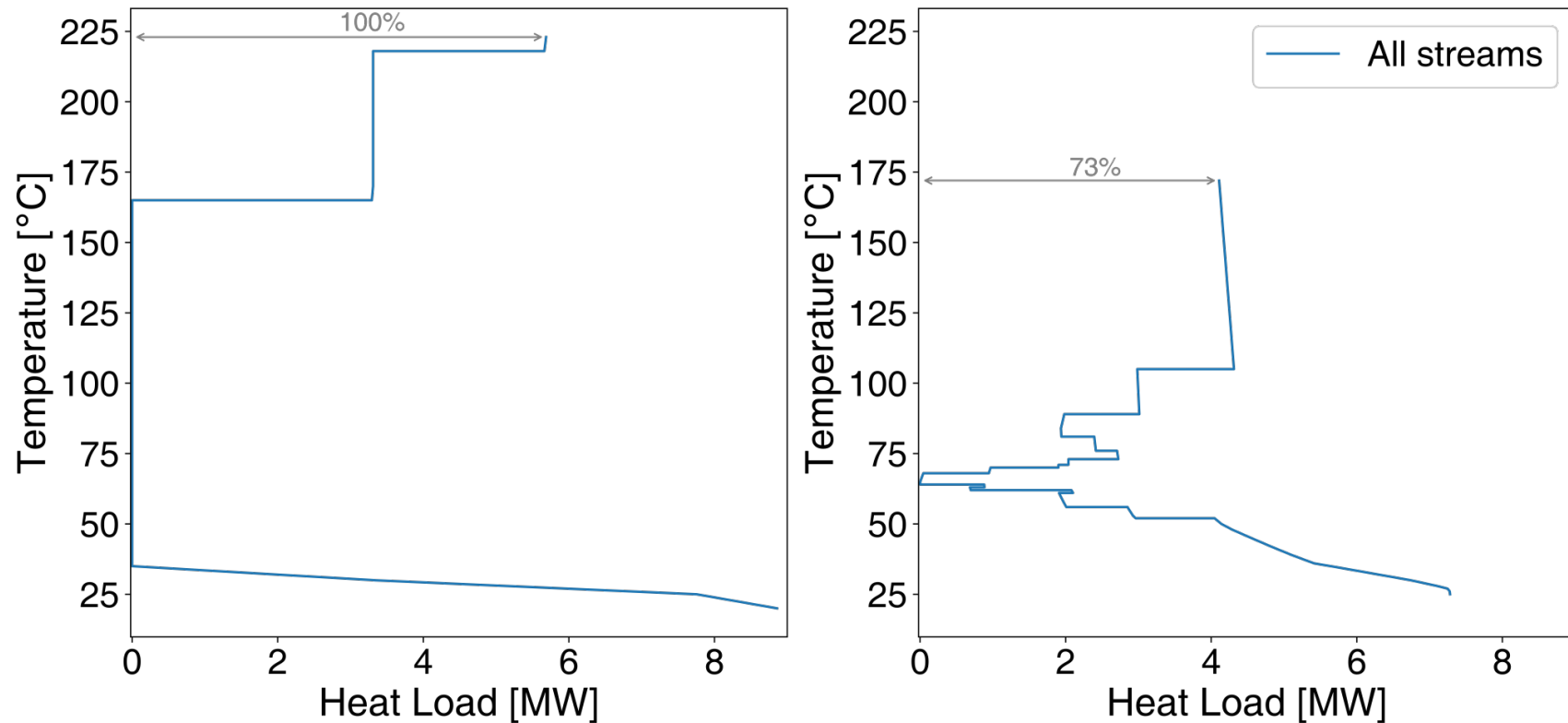


The Grand composite is the heat cascade representation in the corrected temperature domain. it represents the flow of energy in the system from higher temperatures to lower temperature. Above the pinch point is also represents the heat-temperature profile of the heat to be supplied to the system and below the pinch it represents the heat-temperature profile of the heat available in the process and to be removed from the system.

EPFL Heat recovery and heat cascade as a function of the interfaces

8

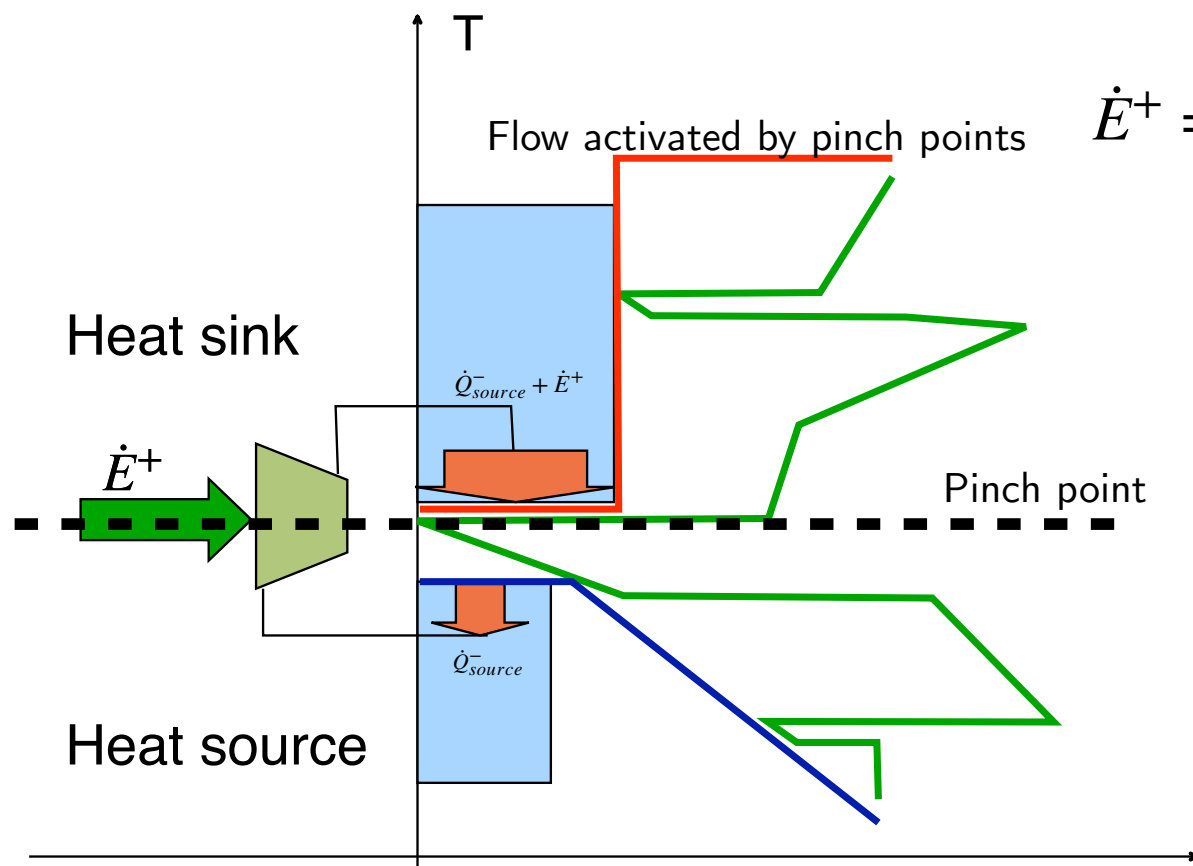
Process integration : utility vs process profiles



- ❖ 27% decrease in hot utility by heat recovery
- ❖ Lower pressure utility
- ❖ cogen or heat pumping ?

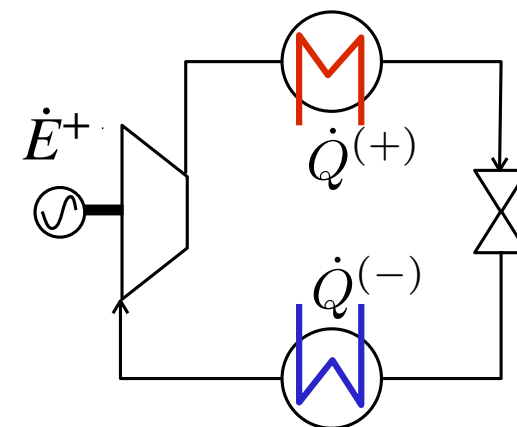
EPFL Integrating heat pumps from heat source to heat sink

$$\text{Savings Hot Utility} = c_{heat}^+ \cdot (\dot{Q}_{source}^- + \dot{E}^+) - c_{elec}^+ \cdot \dot{E}^+$$



$$\dot{E}^+ = \dot{Q}_{sink}^+ \cdot \frac{1}{\eta_{Carnot}} \cdot \frac{\tilde{T}_{sink} - \tilde{T}_{source}}{\tilde{T}_{sink}}$$

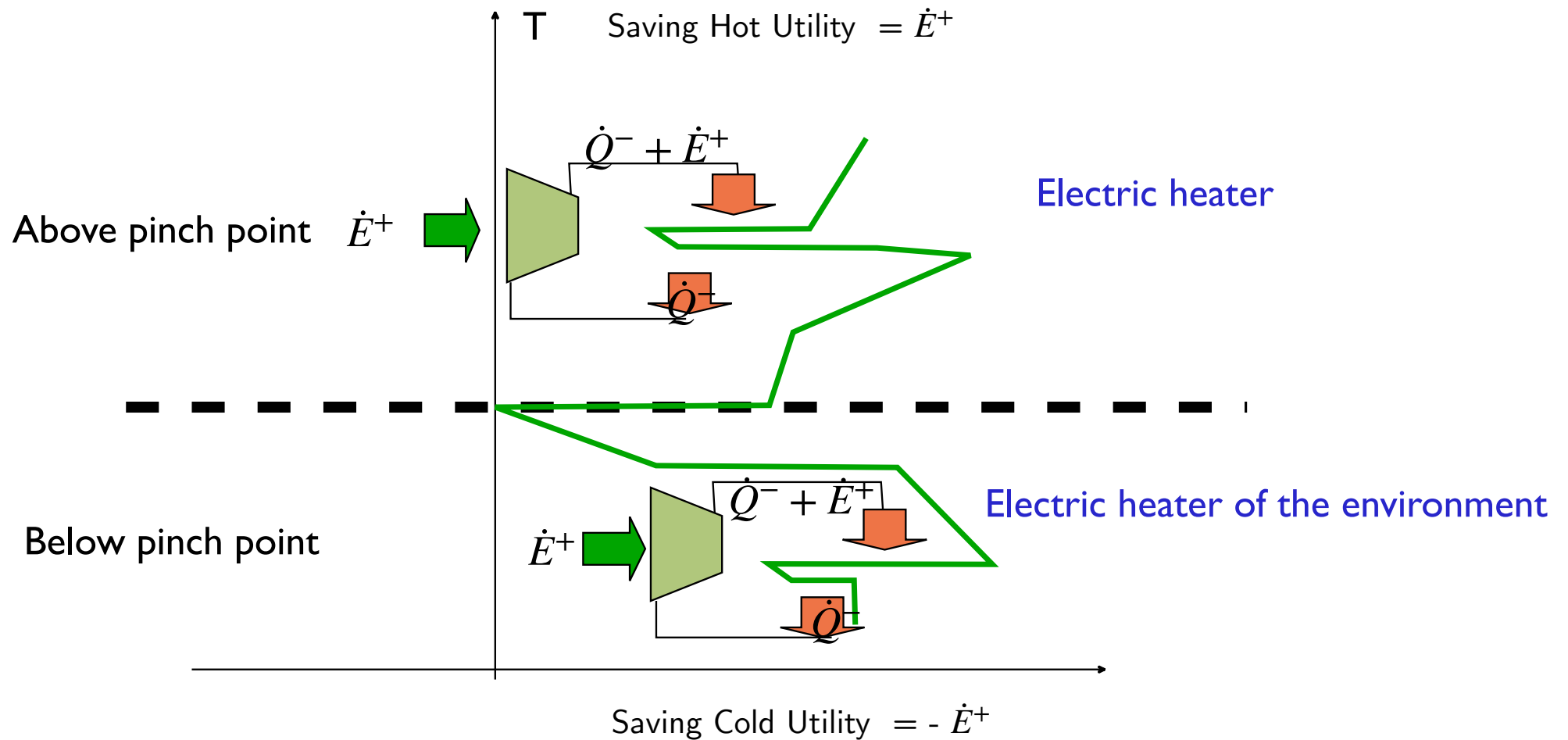
$$\dot{Q}^{(+)} = \dot{W}^+ + \dot{Q}^{(-)}$$



$$\text{Savings Cold Utility} = c_{cold}^+ \cdot \dot{Q}_{source}^-$$

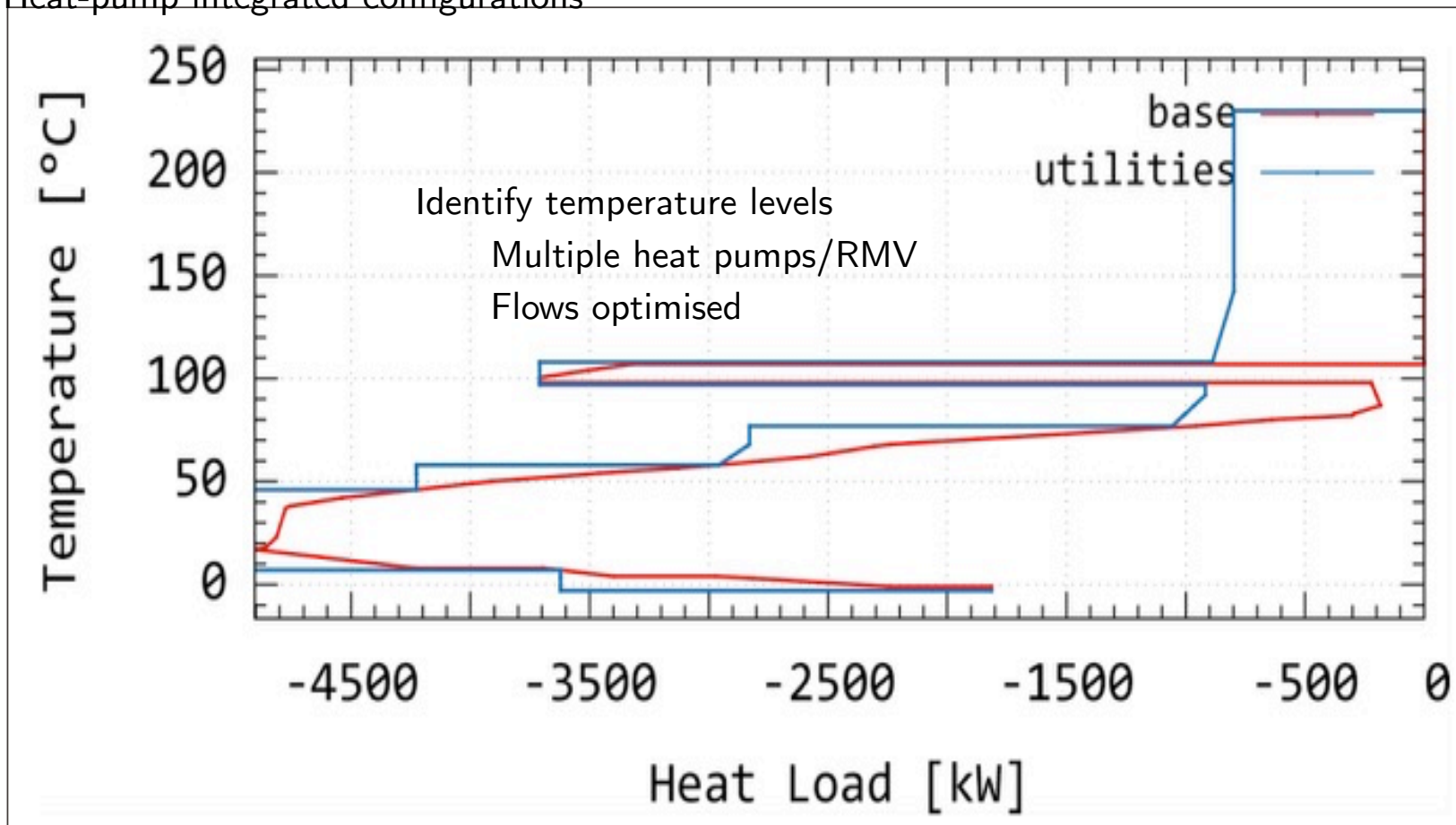
EPFL Miss placed heat pumps : above or below the pinch

10



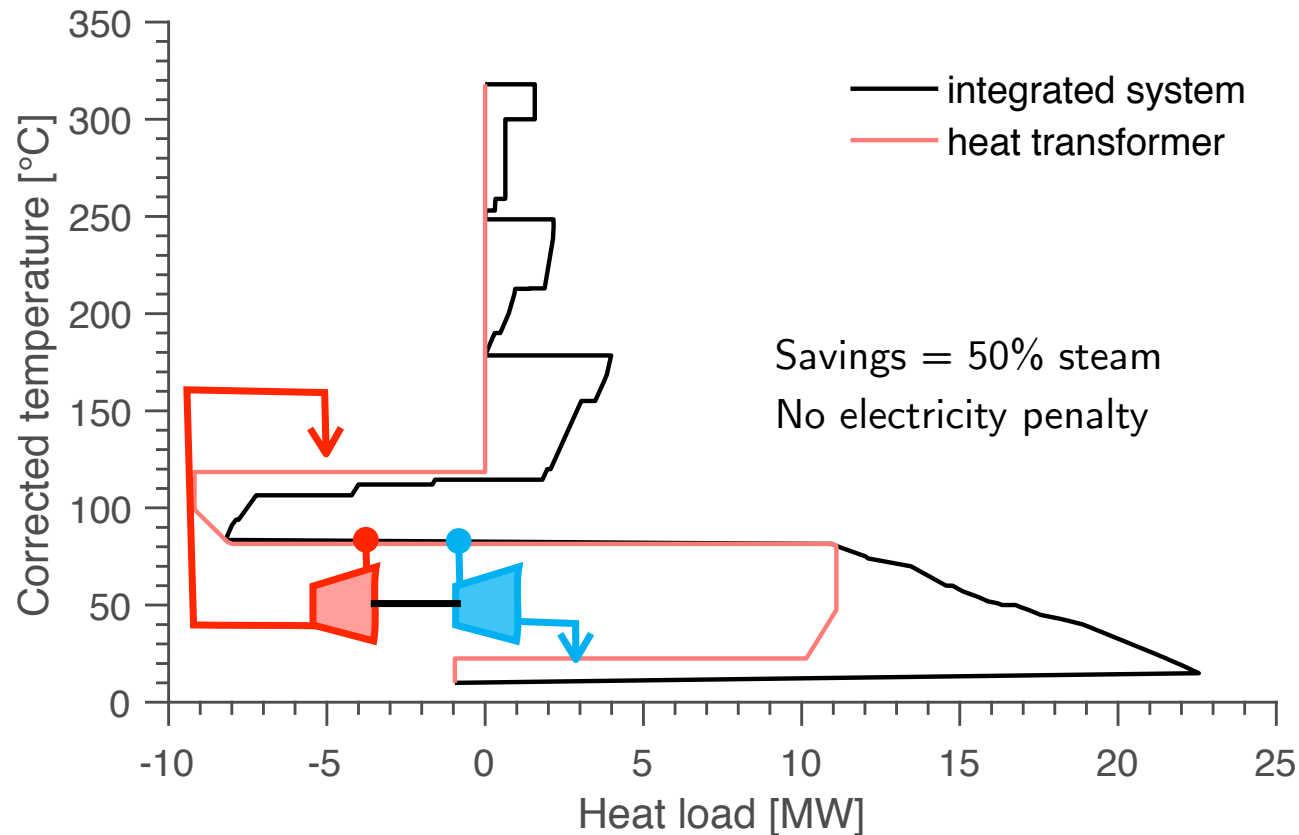
Multi stage heat pump integration

Heat-pump integrated configurations



Wallerand, A. S., Kermani, M., Kantor, I., & Maréchal, F. (2018). Optimal heat pump integration in industrial processes. *Applied Energy*, 219, 68-92.





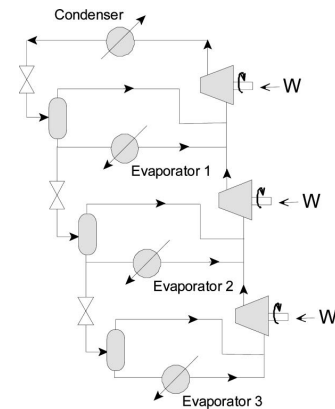
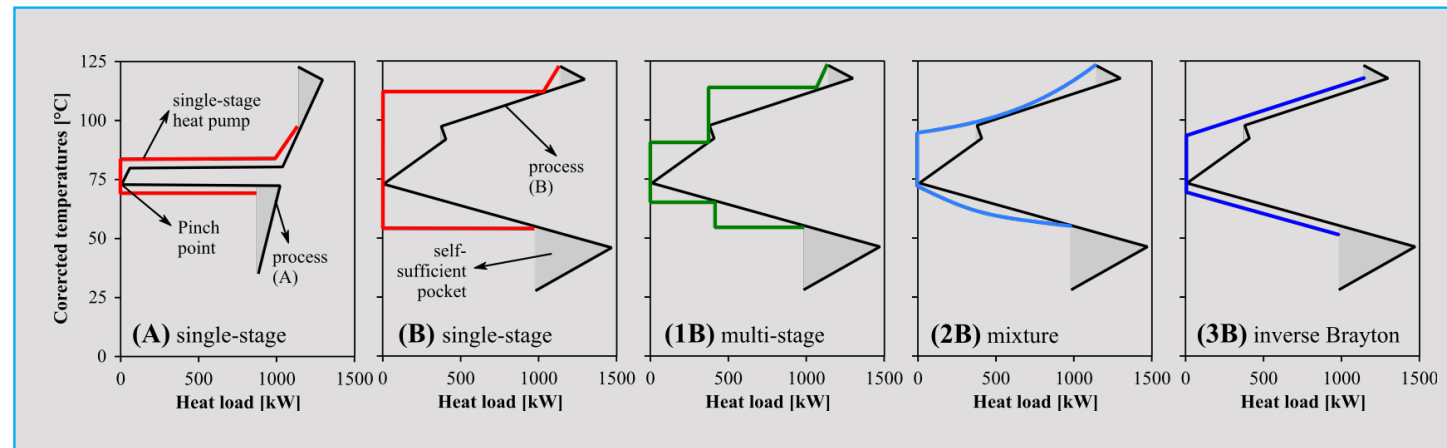
Heat pump + ORC

- Superstructure
- Fluids
- Turbines
- Optimisation

Kermani et al., Applied Energy, 2019

A.S. Wallerand 2018. EPFL Thesis

- Heat pump type ?
- Working fluid ?
- Operating conditions ?
- Multi-stage compression / expansion ?
- Subcooling/preheating ?
- Flash drums ?
- Compressor types ?



All adapted from: Del Nogal et al. (2008)

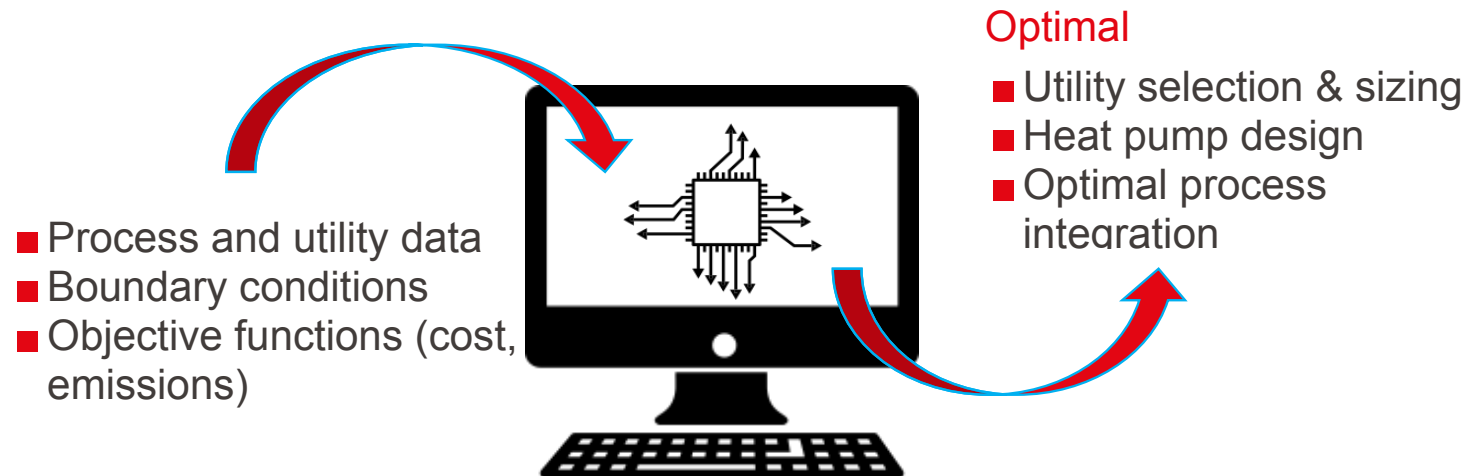
EPFL Systematic approach: superstructure optimisation

14

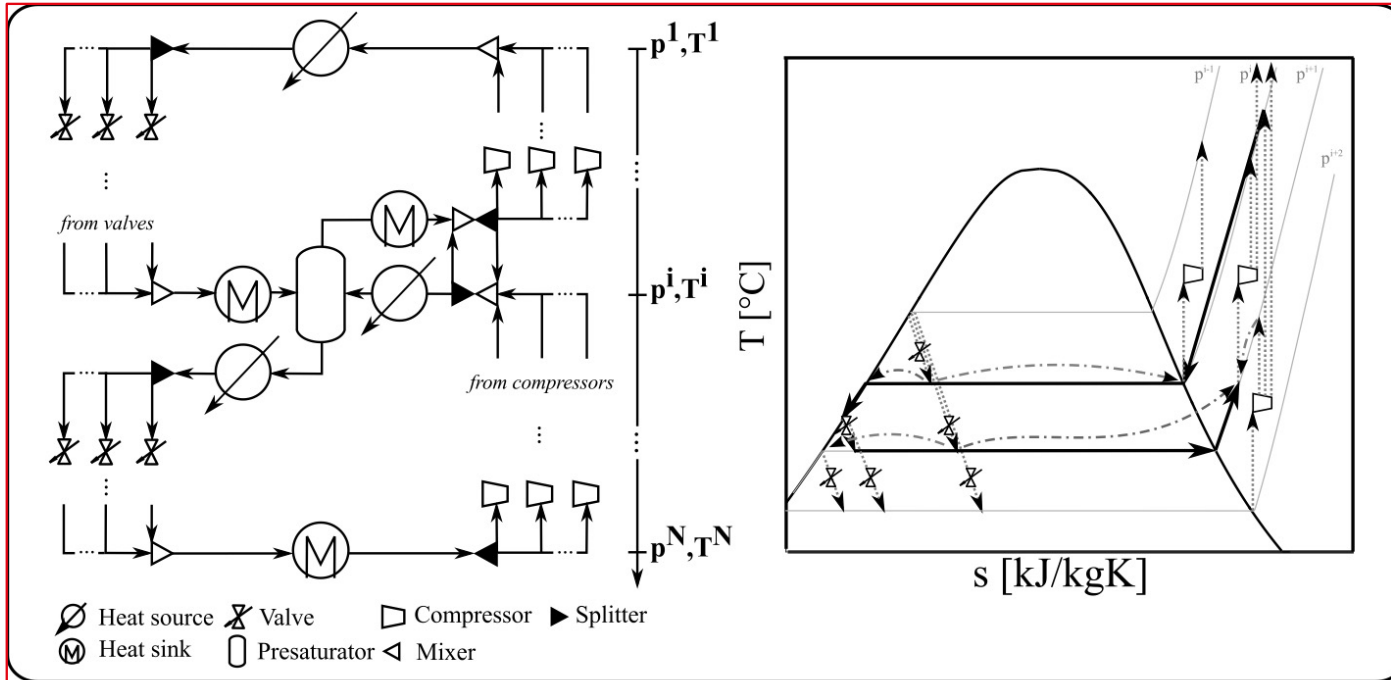
[1] Wallerand et al. 2018

[2] A.S. Wallerand. EPFL Thesis, Lausanne

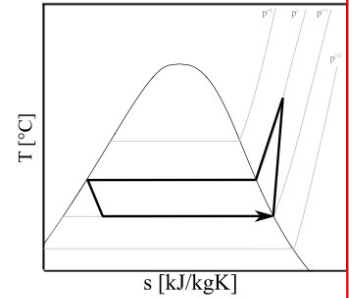
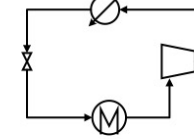
Computer aided process engineering



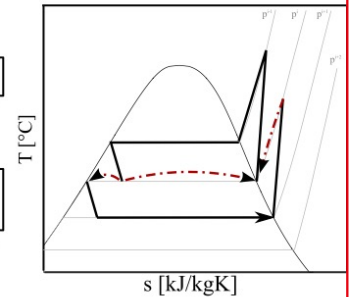
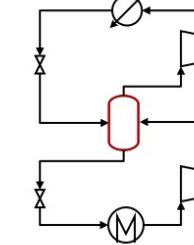
Systematic approach: superstructure model



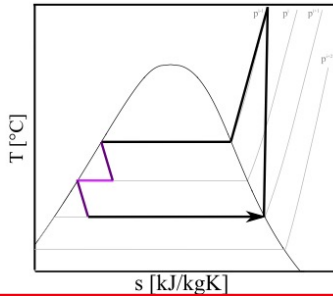
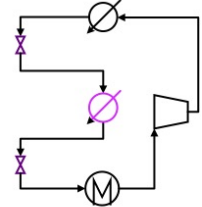
(a) Simple cycle



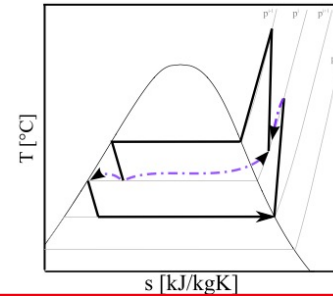
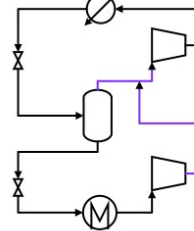
(b) Presaturator



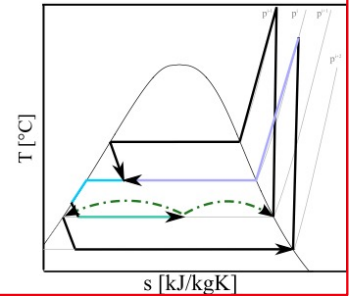
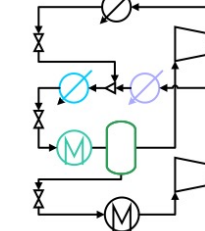
(c) Multi-stage expansion



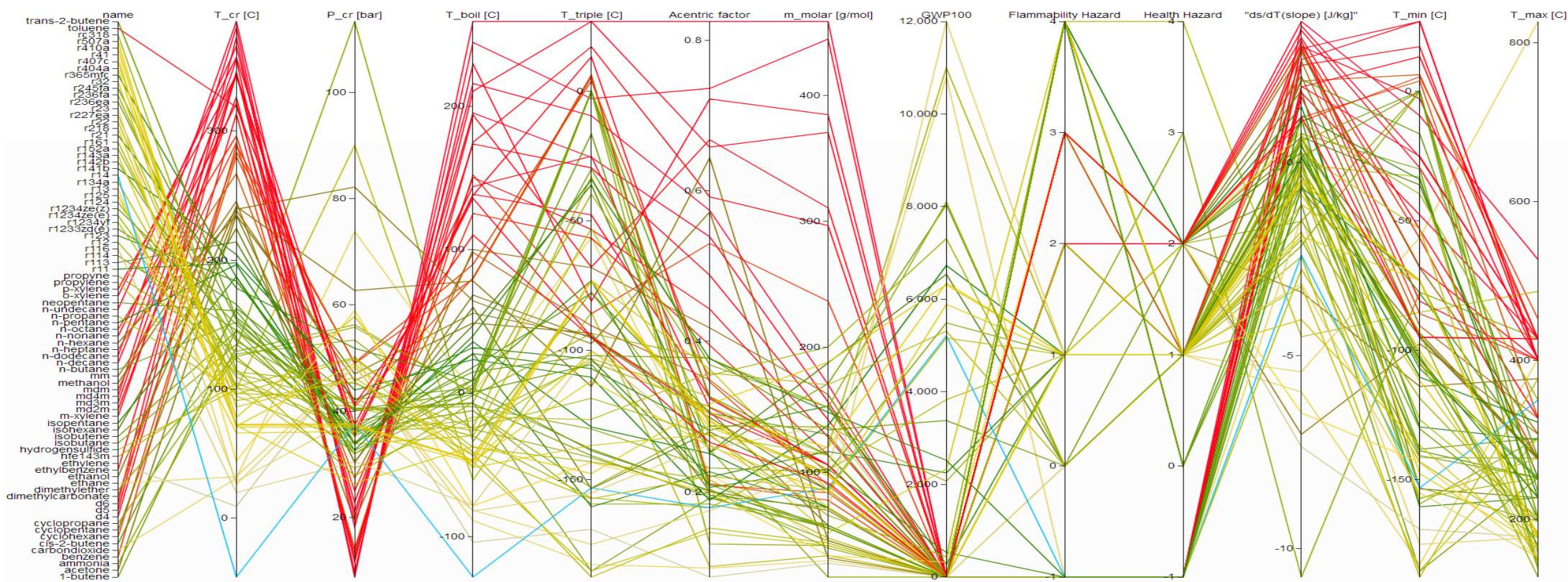
(d) Economizer



(e) Subcooling, presaturator



working fluids and their thermo-physical properties



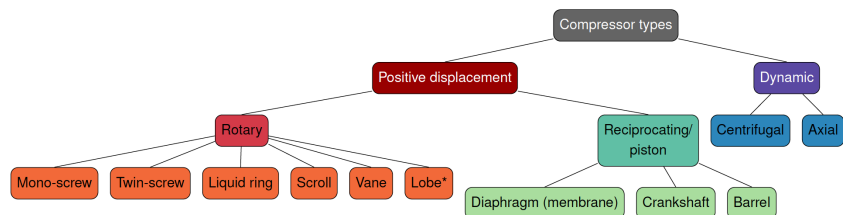
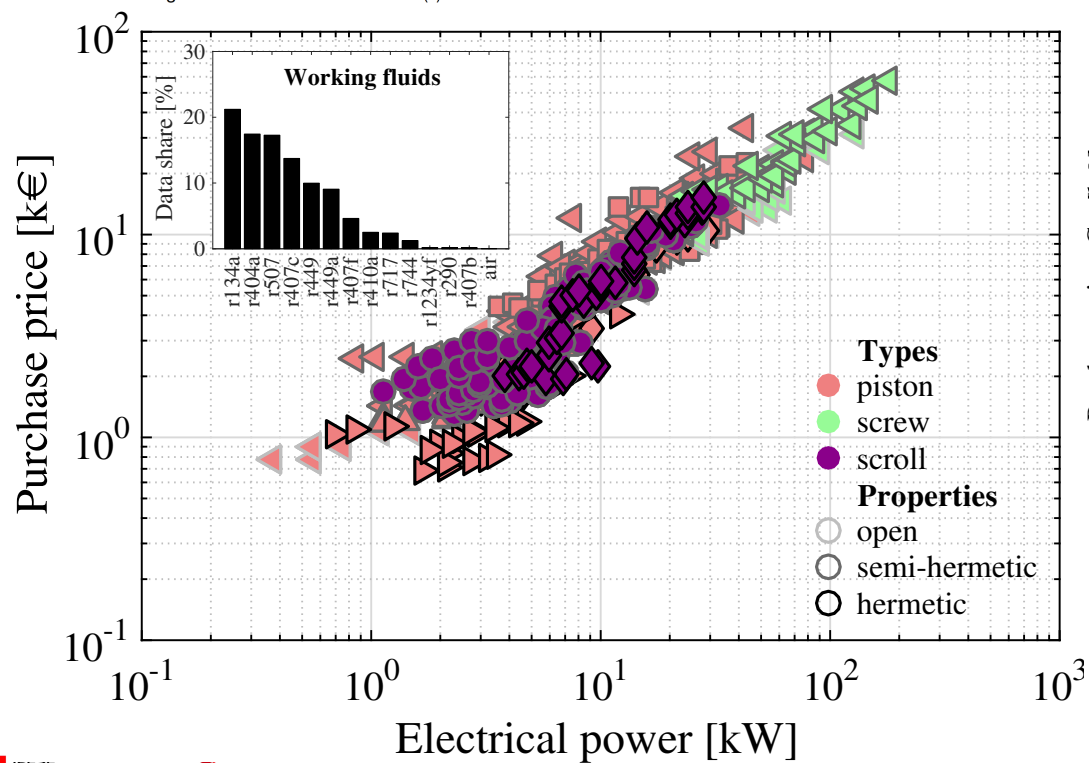
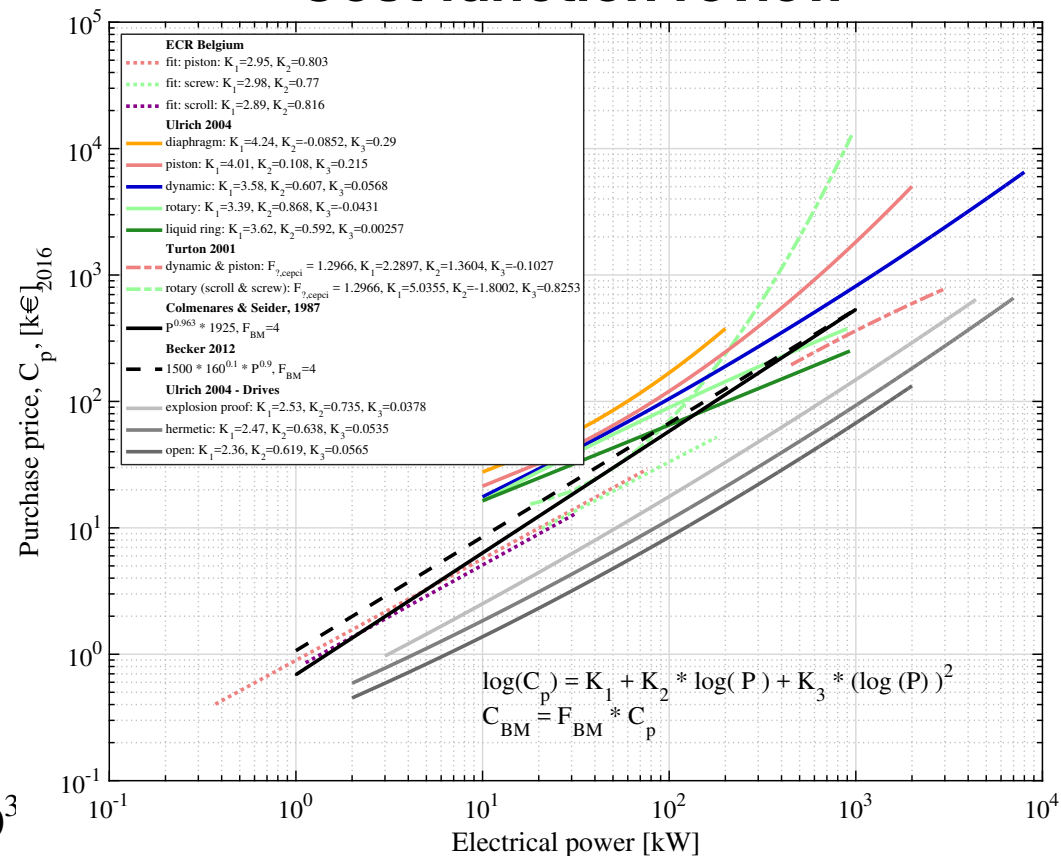


Figure 2: Tree diagram of compressor types, adapted from Wikipedia [8] with inspiration from Favrat [9]. Novel technologies are marked with asterisk (*).



Cost function review



[1] A.Wallerand, BFE 2019

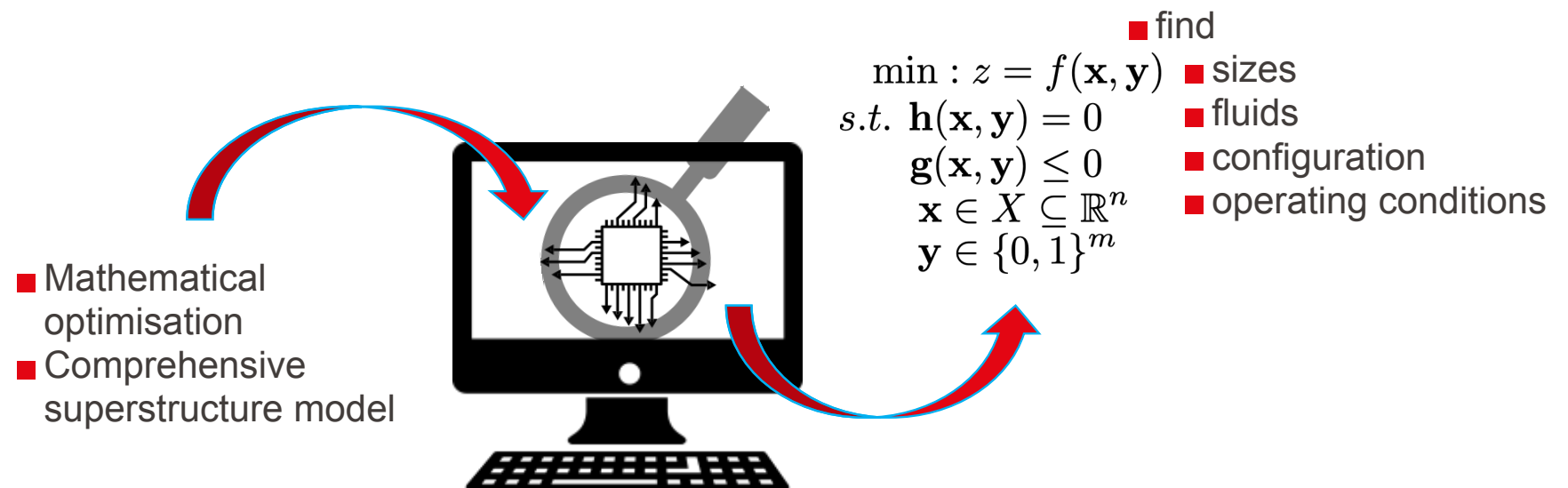
[2] Kantor et al., ECOS proceedings, 2018

EPFL Systematic approach: superstructure optimisation

18

[1] Wallerand et al. 2018

[2] A.S. Wallerand. EPFL Thesis, Lausanne



EPFL Optimisation to select and calculate flows in the system

19

$$\min_{R_r, y_w, f_w, E^+, E^-} \left(\sum_{w=1}^{n_w} C2_w f_w + C_{el+} E^+ - C_{el-} E^- \right) * t \quad \text{Operating cost}$$

$$+ \sum_{w=1}^{n_w} C1_w y_w + \frac{1}{\tau} \left(\sum_{w=1}^{n_w} (CI1_w y_w + CI2_w f_w) \right) \quad \text{Investment}$$

Fixed maintenance

Subject to : Heat cascade constraints

$$\sum_{w=1}^{n_w} f_w q_{w,r} + \sum_{s=1}^{n_s} Q_{s,r} + R_{r+1} - R_r = 0 \quad \forall r = 1, \dots, n_r$$

Feasibility

$$R_r \geq 0 \quad \forall r = 1, \dots, n_r; R_{n_r+1} = 0; R_1 = 0 \quad E^+ \geq 0; E^- \geq 0$$

Electricity consumption

$$\sum_{w=1}^{n_w} f_w e_w + E^+ - E_c \geq 0$$

Electricity production

$$\sum_{w=1}^{n_w} f_w e_w + E^+ - E_c - E^- = 0$$

Energy conversion Technology selection

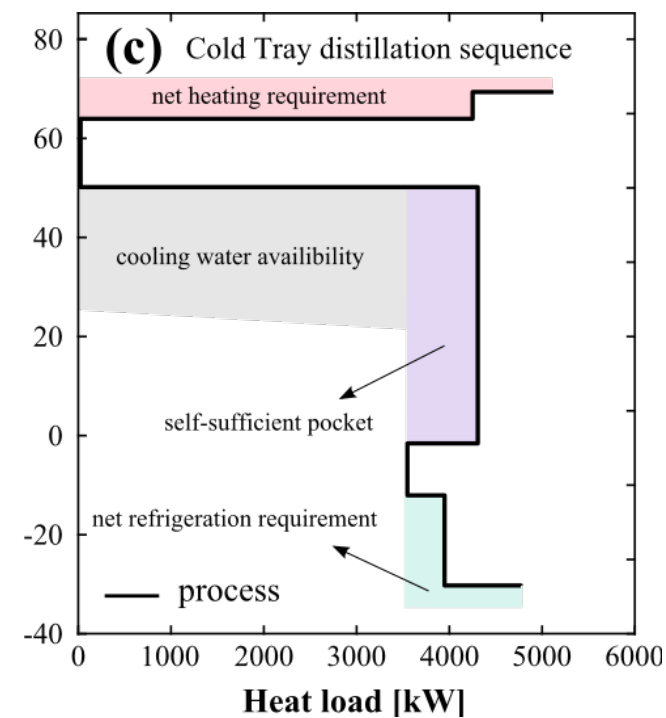
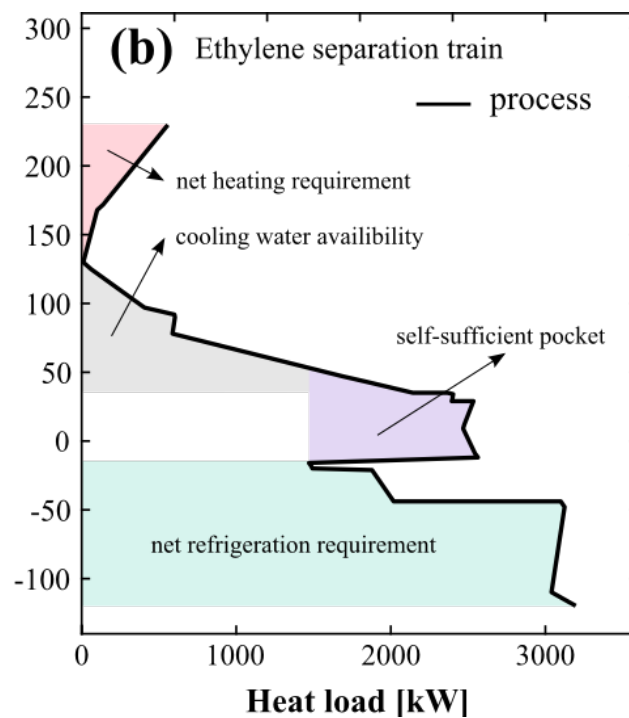
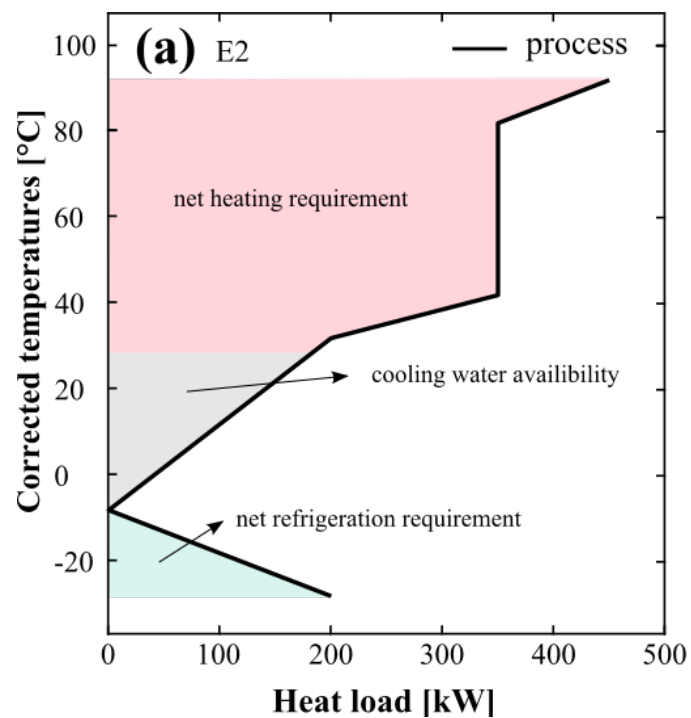
$$fmin_w y_w \leq f_w \leq fmax_w y_w \quad y_w \in \{0, 1\}$$

EPFL Systematic approach: validation

20

[1] Wallerand et al. 2018

[2] A.S. Wallerand. EPFL Thesis, Lausanne



EPFL Systematic approach : validation

21

[1] Wallerand et al. 2018

[2] A.S. Wallerand. EPFL Thesis, Lausanne

[3] Shelton and Grossmann 1986

[4] Colmenares and Seider 1989

[5] Colmenares and Seider 1987

Improvement vs state of the art

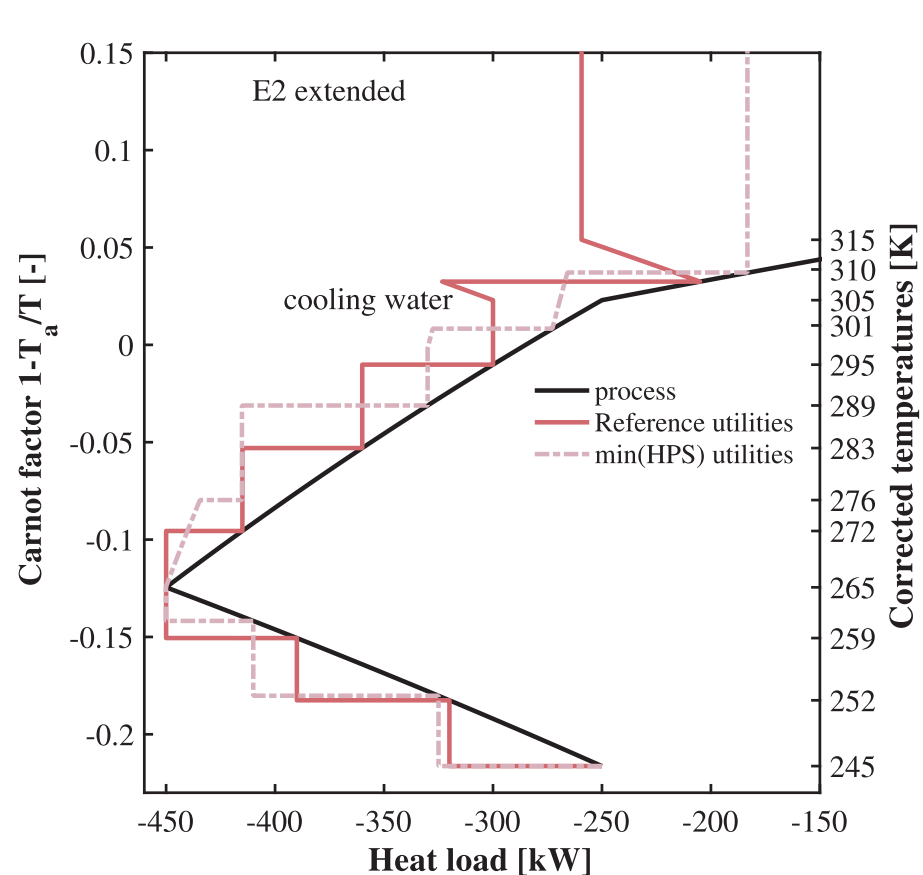
Literature comparison^{1,2}

		<i>E2</i> ^[3]		<i>Ethylene</i> ^[4]		<i>Cold Tray</i> ^[5]	
		Reference	min(HPS)	Reference	min(HPS)	Reference	min(HPS)
Opex							
Cooling water	\$/y	0	0	25,020	23,150	29,930	4,810
Steam	\$/y	10,460	10,370	0	0	287,090	39,310
Electricity	\$/y	27,620	28,040	327,580	223,340	96,370	189,900
Capex							
No. of compressors	#	6	4	5	5	3	5
Compressors	\$/y	54,710	49,630	230,810	159,140	56,380	109,220
TAC	\$/y	92,790	88,050	583,410	405,630	469,770	343,230
Improvement	%	0	5.1%	0%	30.5%	0%	26.9%
COP _{refrigeration}	-	4.4	4.3	1.8	2.6	5.3	5.8

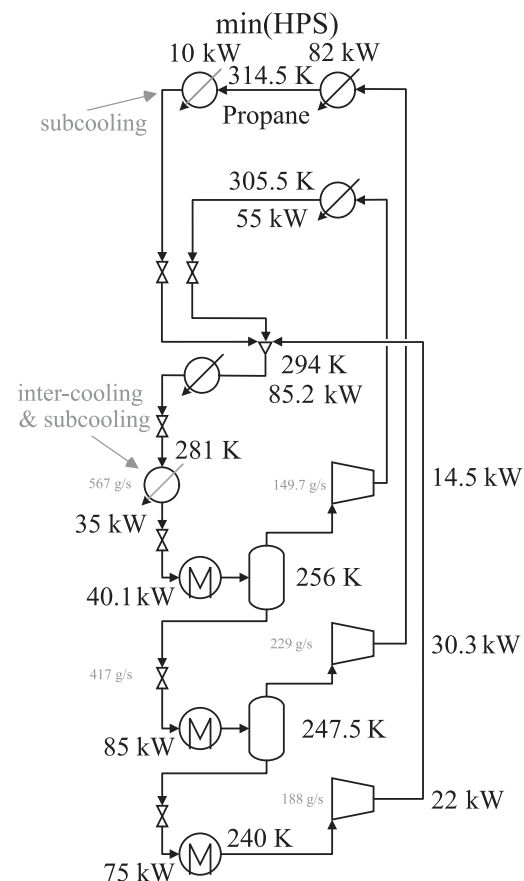
EPFL A multiple levels heat pumping system integration

22

CARNOT Integrated composite curves : the area between the two curves defines the exergy losses in the heat transfer



(a) Integrated composite curves of optimized and reference case.



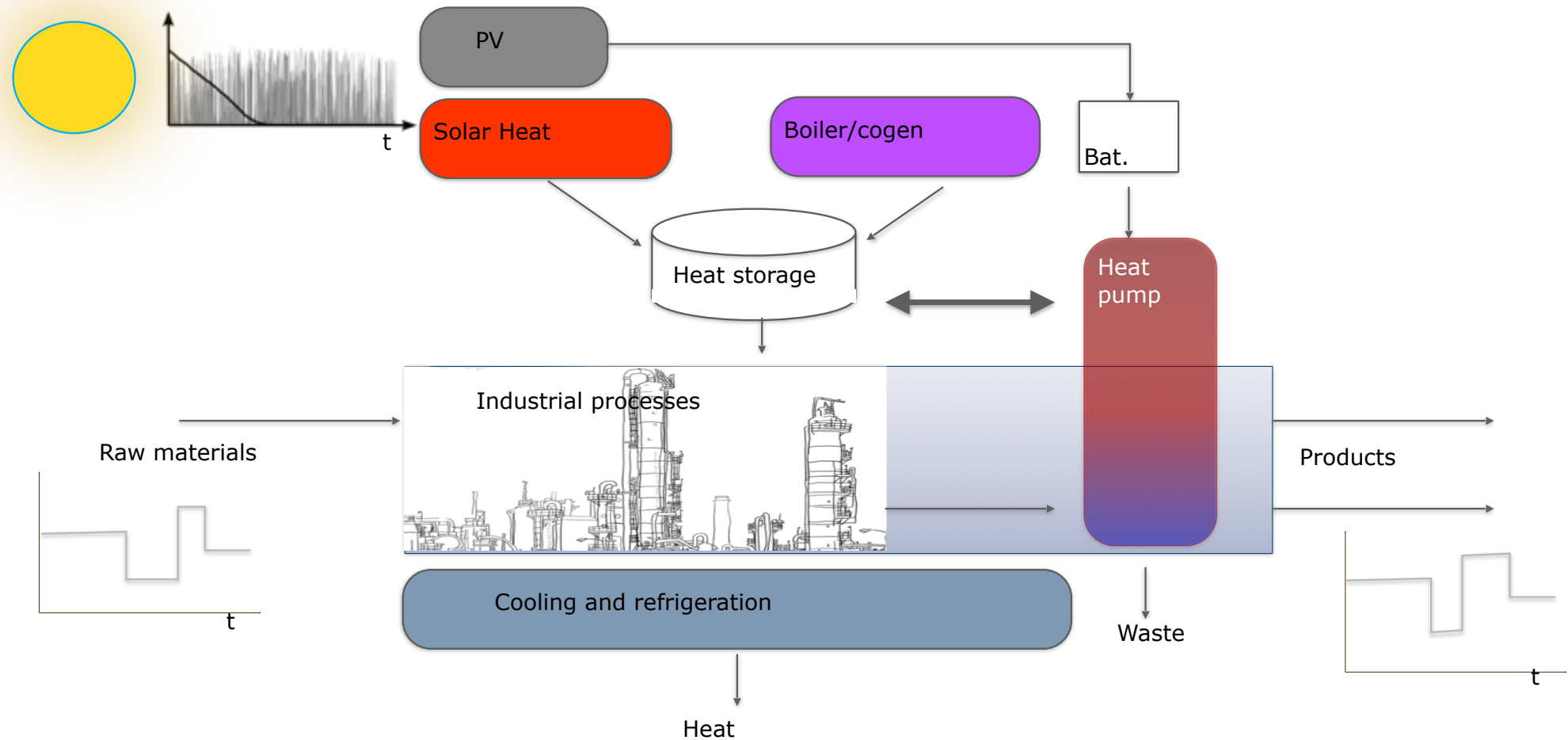
(b) Flowsheet of optimum case.

Fig. 15. Extended case E2 minimum TAC solution.

[1] Wallerand et al. 2018

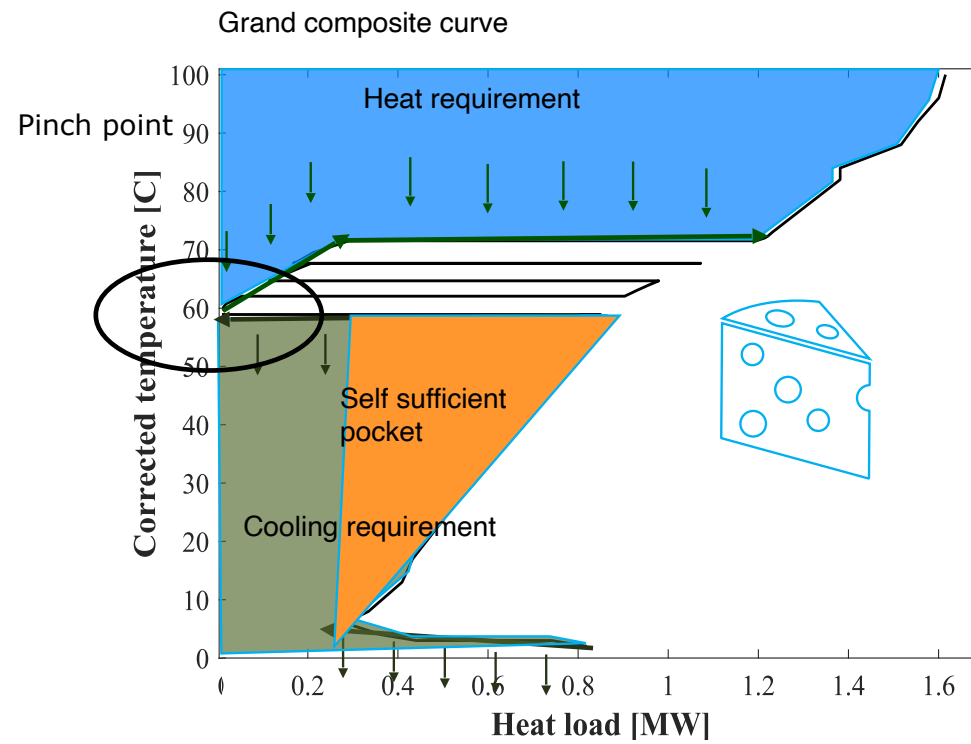
EPFL Integrating renewable energy

23



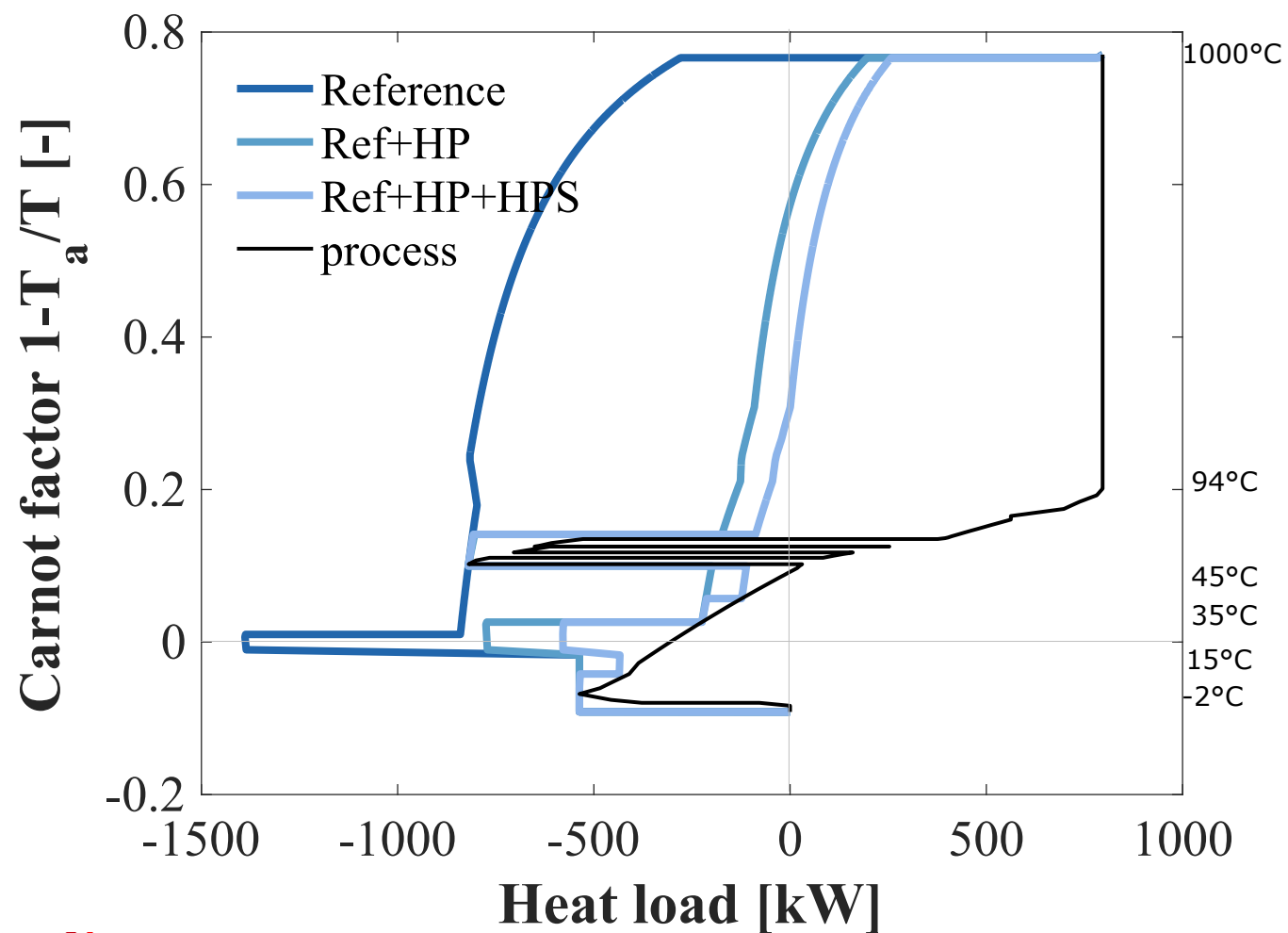
EPFL Dairy process

24

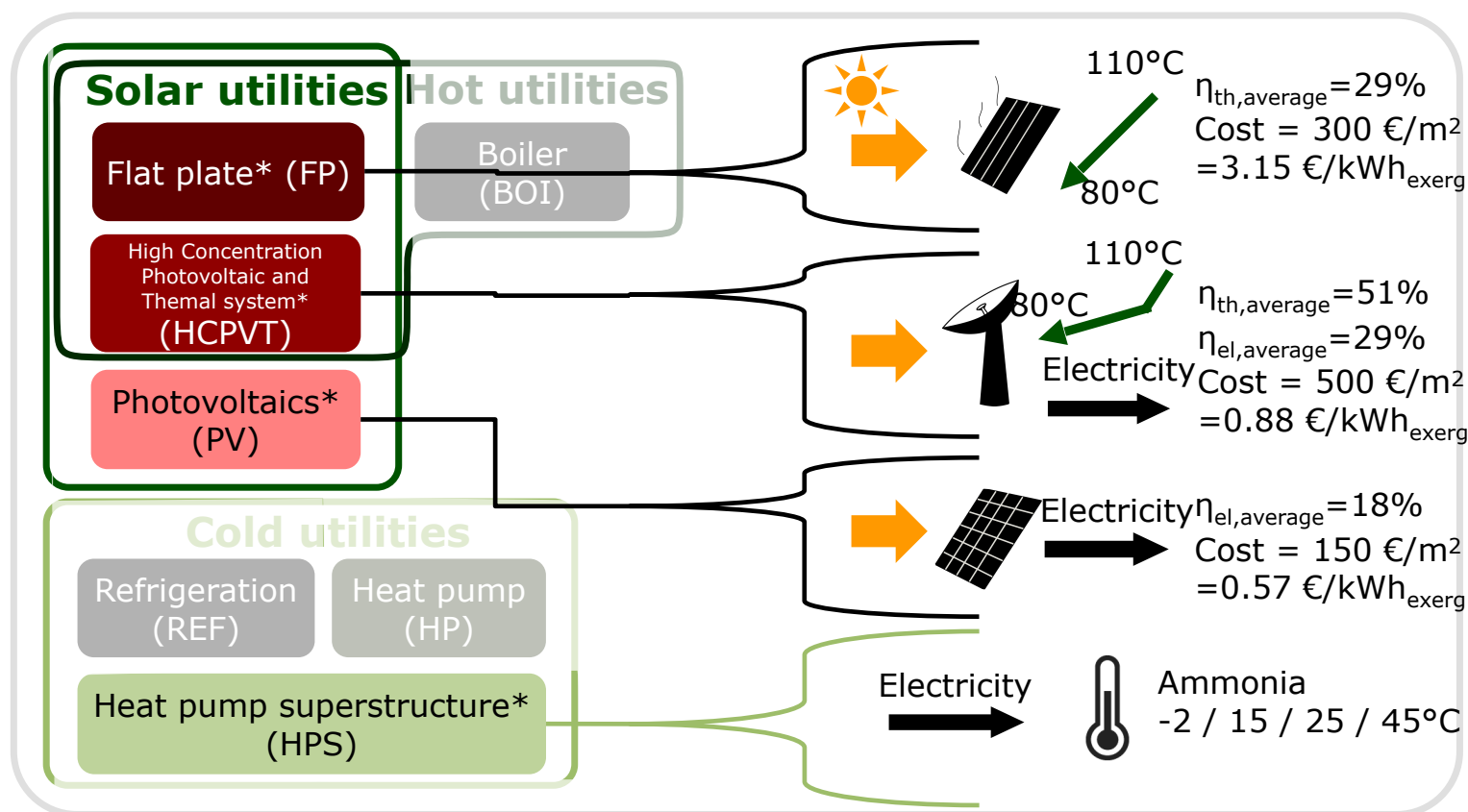


Dairy case study: heat pump integration

Exergy integrated composite curves



Case study: Solar energy and heat-pumps



(1) Tehnomont, Solarna Oprema Pula. SKT 100; (2) SunTech, HyPro, STP 290S-20; (3) Airlight Energy Holding SA

Targeting problem : multi-period problem

$$\min_{R_p^p, y_p^p, u_p^p, y_p^{\max}, u_p^{\max}} \sum_{p=1}^P \left(\sum_{w=1}^W \text{OP}_{1,p}^w \cdot y_p^w + \text{OP}_{2,p}^w \cdot u_p^w \right) \cdot \Delta t_p \cdot \text{occ}_p + \text{ann} \cdot \sum_{w=1}^W \text{IV}_1^w \cdot y^{w,\max} + \text{IV}_2^w \cdot u^{w,\max}$$

$$u_p^w \in \mathbb{C}^+ \quad \forall w \in W, p \in P$$

$$y_p^w \in \{0,1\} \quad \forall w \in W, p \in P$$

$$P = \{1, 2, 3, \dots, 240\}$$

subject to

heat cascade constraints:

$$\sum_{w=1}^W u_p^w \cdot Q_{p,r}^w + \sum_{s=1}^S Q_{s,r} \cdot L_{s,r} + R_{p,r+1} - R_{p,r} = 0 \quad \forall p \in P, r \in \text{RT}$$

thermodynamic feasibility:

$$R_{p,1} = 0, R_{p, N_{\text{RT}}+1} = 0, R_{p,r} \geq 0 \quad \forall r \in 1, \dots, N_{\text{RT}} + 1, p \in P$$

maximum size of operation and existence of technology w:

$$\left. \begin{array}{l} u^{w,\max} - u_p^w \geq 0 \quad \forall w \in W, p \in P \\ y^{w,\max} - y_p^w \geq 0 \quad \forall w \in W, p \in P \end{array} \right| U^{w,\min} \cdot y_p^w \leq u_p^w \leq U^{w,\max} \cdot y_p^w \quad \forall w \in W, p \in P$$

Solar technologies

$$u^{ws,\max} - u_p^{ws} = 0 \quad \forall ws \in W_s, p \in P$$

EPFL Targeting problem : multi-period + storage problem

28

$$\min_{R_r^p, y_w^p, u_w^p, y_w^{\max}, u_w^{\max}} \sum_{p=1}^P \left(\sum_{w=1}^W \text{OP}_{1,p}^w \cdot y_p^w + \text{OP}_{2,p}^w \cdot u_p^w \right) \cdot \Delta t_p \cdot \text{occ}_p + \text{ann} \cdot \sum_{w=1}^W \text{IV}_1^w \cdot y^{w,\max} + \text{IV}_2^w \cdot u^{w,\max}$$

$$u_p^w \in \zeta^+ \quad \forall w \in W, p \in P$$

$$y_p^w \in \{0,1\} \quad \forall w \in W, p \in P$$

$$P = \{1, 2, 3, \dots, 240\}$$

subject to

Storage model

$$M_{S,t} - M_{0,S} = \sum_{st=1}^t d_t \cdot \left(\dot{M}_{h,S,st} + \dot{M}_{h_{losteq},S,st} - \dot{M}_{c,S,st} \right)$$

$$S \in STO : S = 1, \forall t = 1, \dots, T$$

$$M_{S,t} - M_{0,S} = \sum_{ts=1}^t d_{ts} \cdot \left(\dot{M}_{c,S-1,ts} + \dot{M}_{h,S,ts} + \dot{M}_{h_{losteq},S,ts} - \dot{M}_{c,S,ts} + \dot{M}_{h,S+1,ts} - \dot{M}_{h_{losteq},S-1,ts} \right)$$

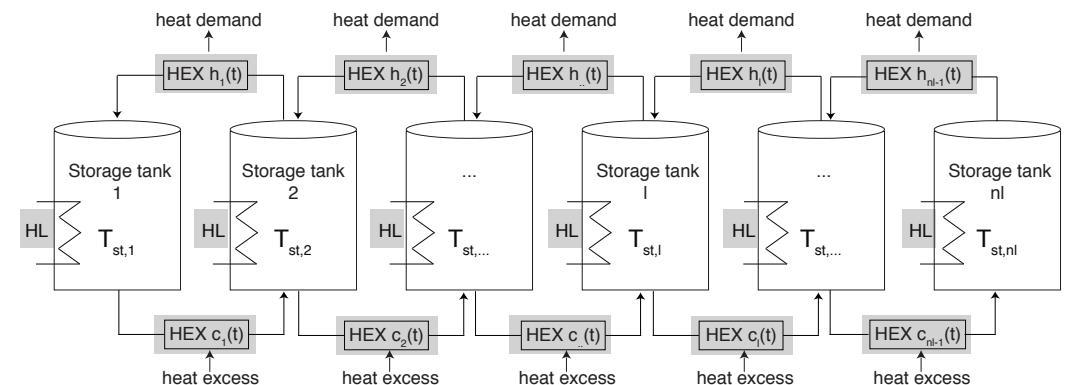
$$\forall S \in STO : S = 2, \dots, N_S - 1, \forall t = 1, \dots, T$$

$$M_{S,t} - M_{0,S} = \sum_{ts=1}^t d_{ts} \cdot \left(\dot{M}_{c,S-1,ts} - \dot{M}_{h,S-1,ts} - \dot{M}_{h_{lost},S-1,ts} \right)$$

$$\forall S \in STO, S = N_S, \forall t = 1, \dots, T$$

$$y_u^t = 0 - 1$$

$$y_u = 0 - 1 \quad \forall u \in FU$$

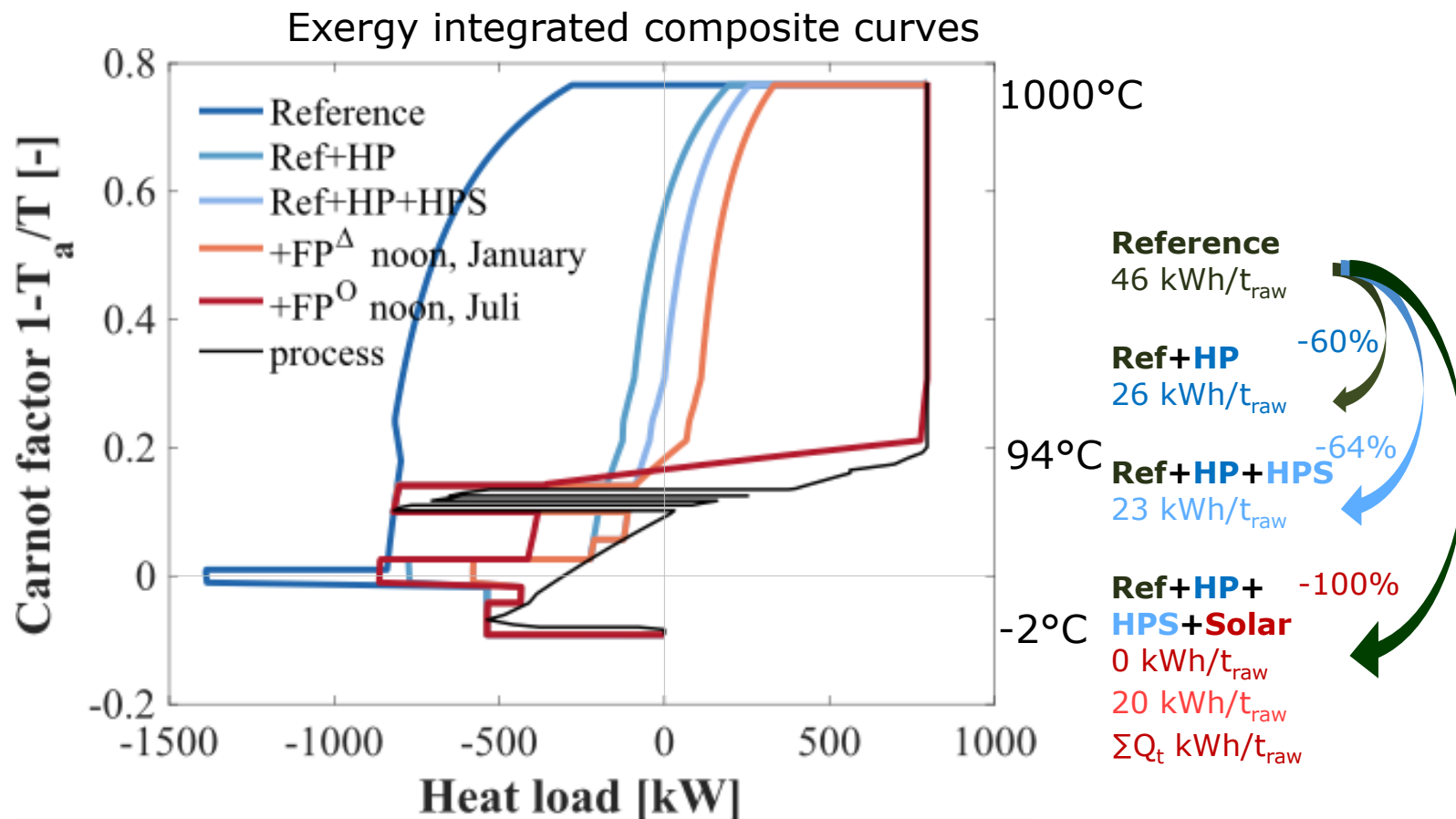


Units for heat integration

HEX: Heat exchangers
HL: Heat losses

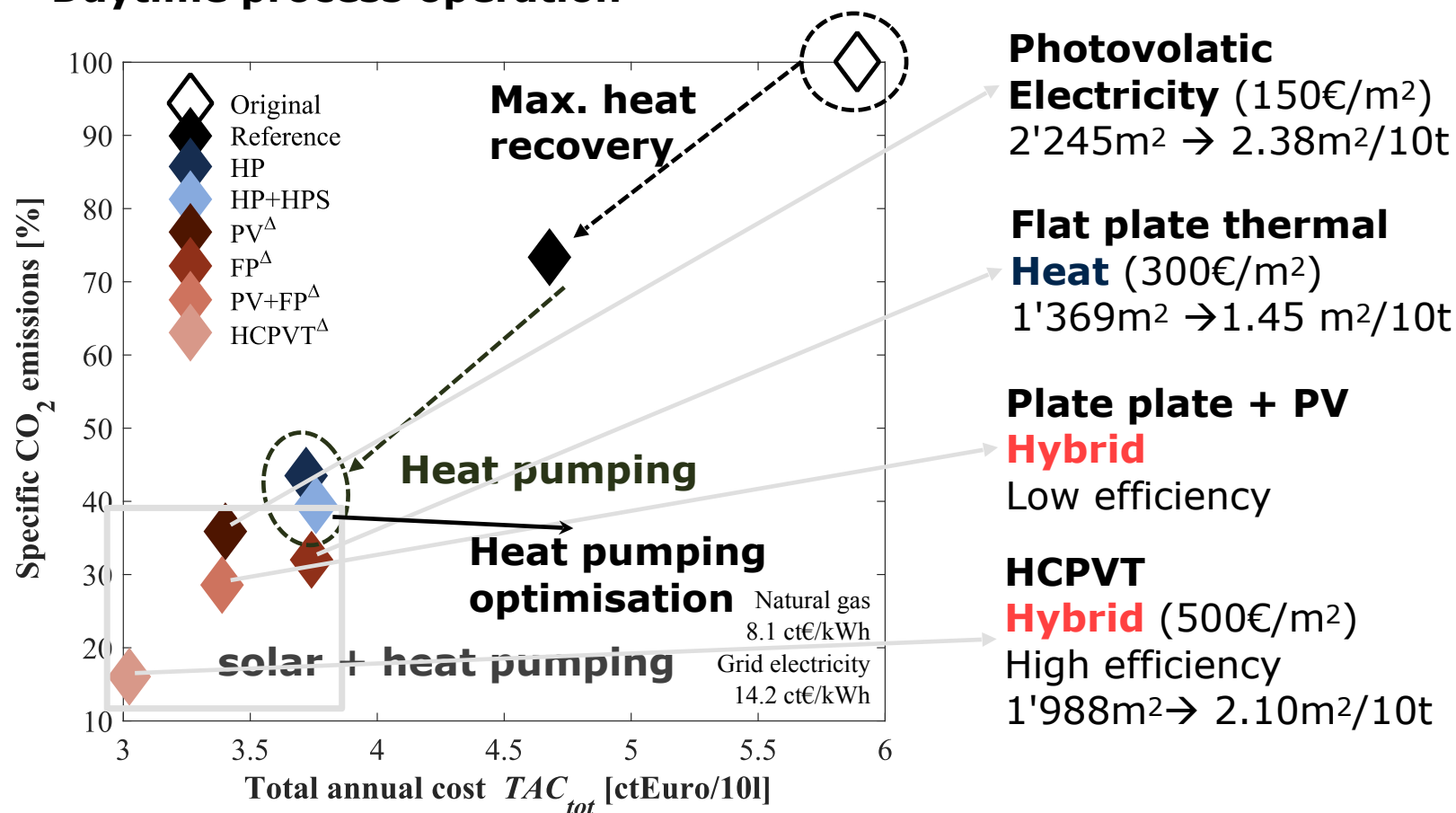
EPFL Integrating solar heat

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Comparison of the different solutions

Daytime process operation



Connected to the grid : optimal predictive strategic operation



Status of inventory+ equipment

Electricity mix predictions

50 hours ahead prediction (ENTSOE)

Minimisation of the energy consumption

Utility market

Electricity consumption [MWh]	Operating cost [EUR]	CO2 emissions [kgCO2eq]
-------------------------------	----------------------	-------------------------

32.3

745.5

958.5

Minimisation of the operating cost

Electricity market

Electricity consumption [MWh]	Operating cost [EUR]	CO2 emissions [kgCO2eq]
-------------------------------	----------------------	-------------------------

32.3

640.1

870.2

-14.2 %

Minimisation of CO2 equivalent emissions

CO2 market

Electricity consumption [kWh]	Operating cost [EUR]	CO2 emissions [gCO2eq]
-------------------------------	----------------------	------------------------

32.3

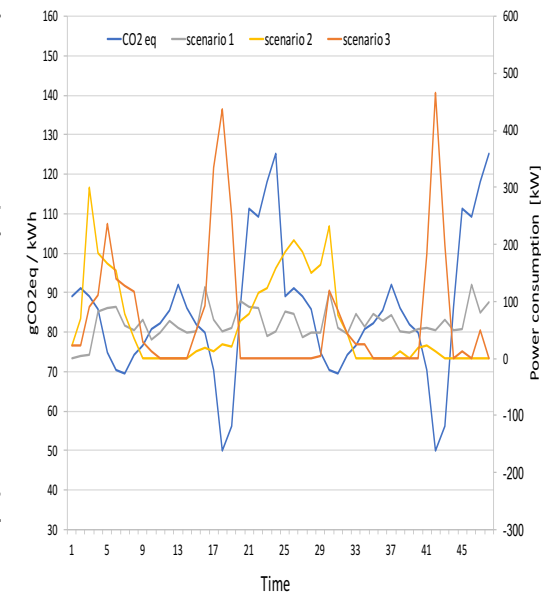
747.5

690.0

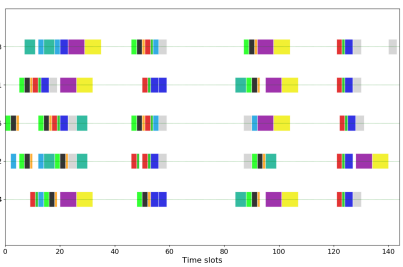
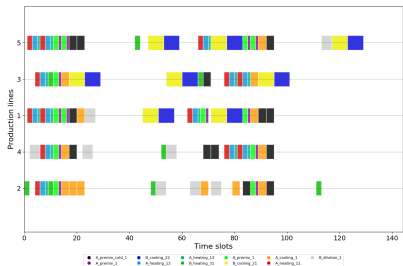
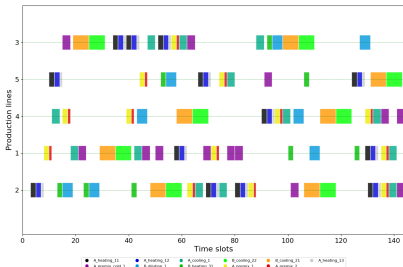
-27.9 %

Strategic planning

integrating with the electricity mix



Santecchia et al, 2019 under preparation



Conclusions : industrial heat pump integration

- Process integration of industrial heat pumps
 - System pinch is the key
 - System boundaries
 - integrate waste treatment and urban integration
 - Heat pumps integrates with other utilities
 - cogeneration - waste heat valorisation
 - Heat storage and optimal strategic operation
- Methods
 - System energetics analysis
 - Heat exchange interfaces
 - Grand composite => temperature levels
 - Super-structure => fluids + system configuration for temperature levels
 - Optimisation => selection and flows
 - Integrated composite curves => exergy losses

- (1) Wallerand, A. S.; Kanton, I.; Maréchal, F. Impact and Role of Innovative Integrated Industrial Heat Pump Systems in the Energy Transition; Swiss Federal Office of Energy SFOE, 2020.
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